

Improvement of Mechanical Properties and Life Extension of High Reliability Structural Components by Laser Shock Processing

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Improvement of Mechanical Properties and Life Extension of High Reliability Structural Components by Laser Shock Processing

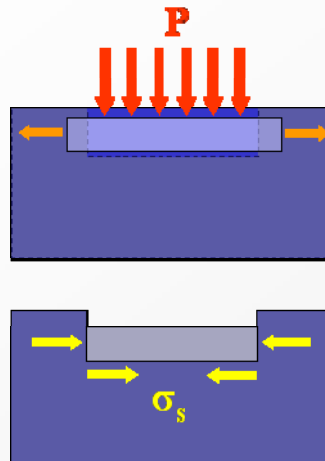
OUTLINE:

- Introduction. Fundamental Physics of Laser Shock Processing
- Experimental Procedure
- Experimental Results for Al2024-T351 and Ti6Al4V
 - Surface Roughness
 - Microstructure
 - Microhardness
 - Wear
 - Residual stresses
 - Fatigue crack growth
- Discussion and Outlook

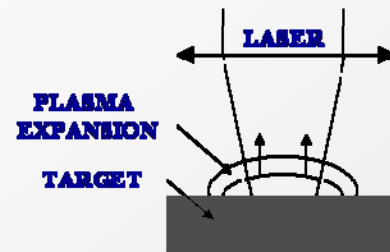
INTRODUCTION

- Laser Shock Processing (LSP) is developed as a technique allowing the effective induction of residual stresses fields in metallic materials allowing a high degree of surface material protection against fatigue crack propagation, abrasive wear, chemical corrosion and other failure conditions, what makes the technique specially suitable and competitive with presently use techniques for the treatment of heavy duty components in the aeronautical, nuclear and automotive industries.
- However, according to the inherent difficulty for the prediction of the shock waves generation (plasma) and evolution in treated materials, the practical implementation of LSP processes needs an effective predictive assessment capability coupled to a readily controllable experimental setup for a correct application of treatment parameters and an associate material properties characterization capability.
- Despite the availability of the LSP technique at laboratory level, practical developments at industrial level still need to be further accomplished.
- In the present communication, the practical LSP treatment and associate specimens characterization capabilities developed at CLUPM (Spain) are presented along with selected results obtained in two relevant aerospace alloys (Al2024-T351 and Ti6Al4V).

REMINDER OF LSP PHYSICAL PRINCIPLES (1/2)

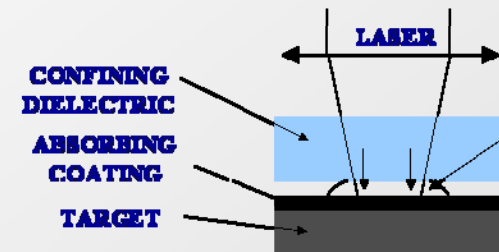


FREE MODE

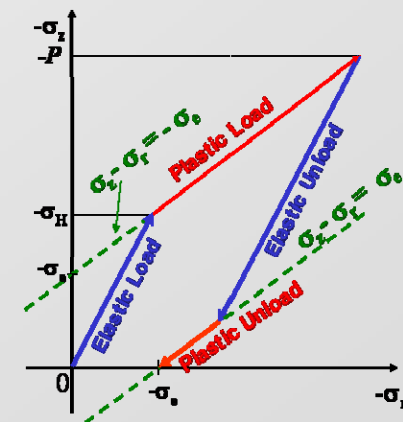
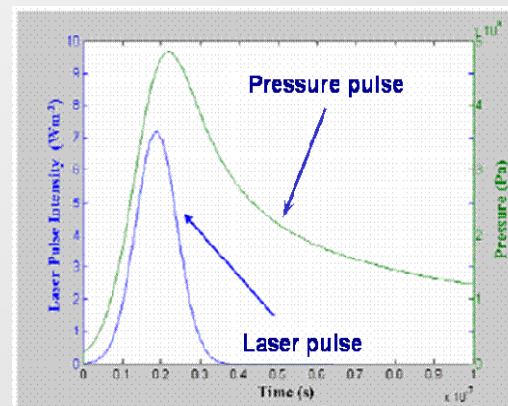
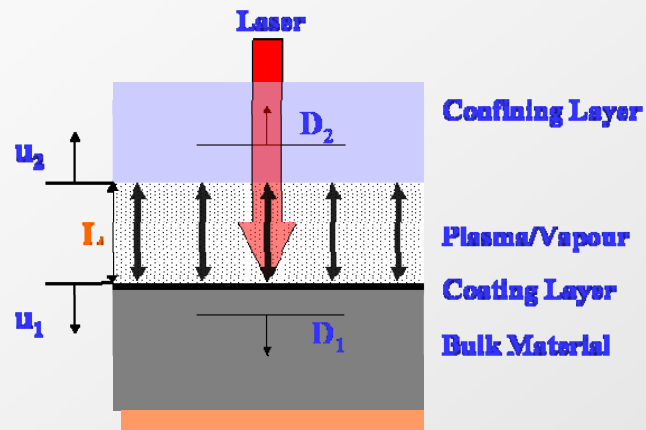


FREE PLASMA EXPANSION

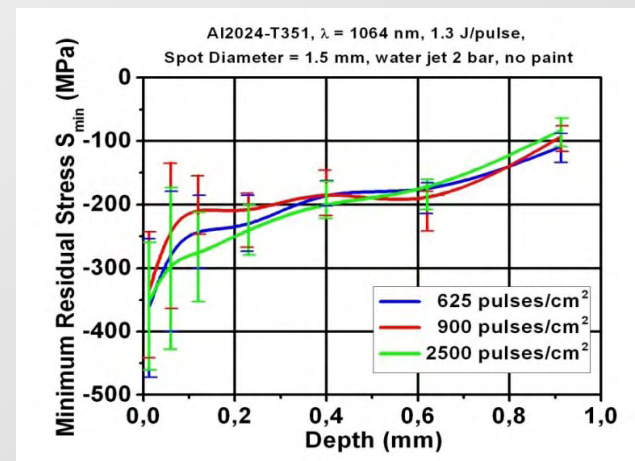
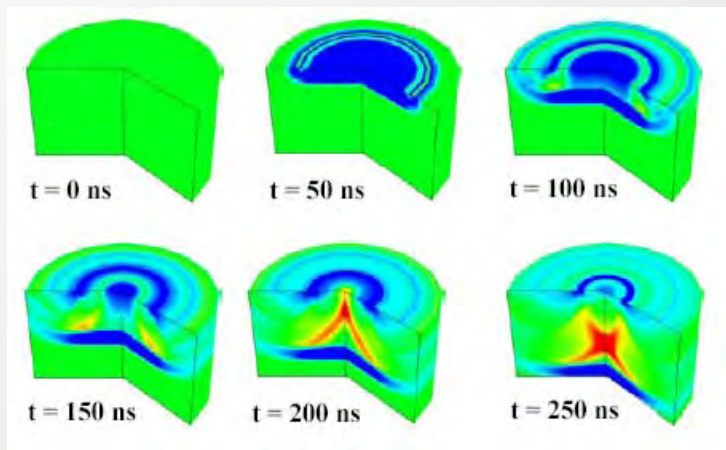
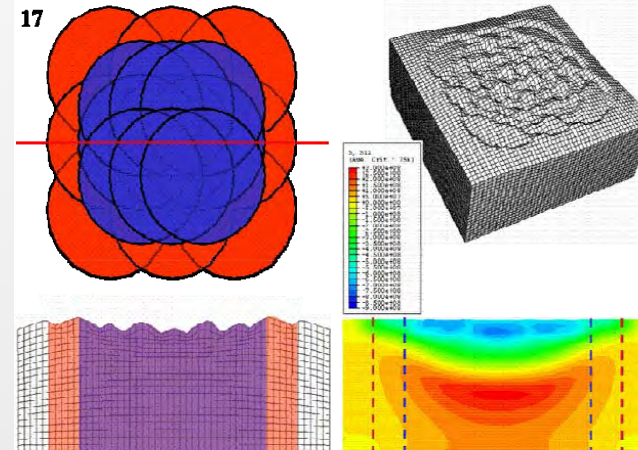
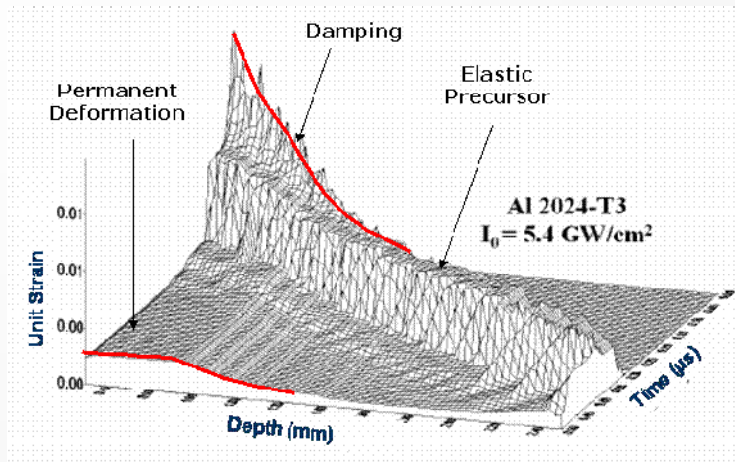
CONFINED MODE



IMPROVED PRESSURE AND IMPULSION



REMINDER OF LSP PHYSICAL PRINCIPLES (2/2)



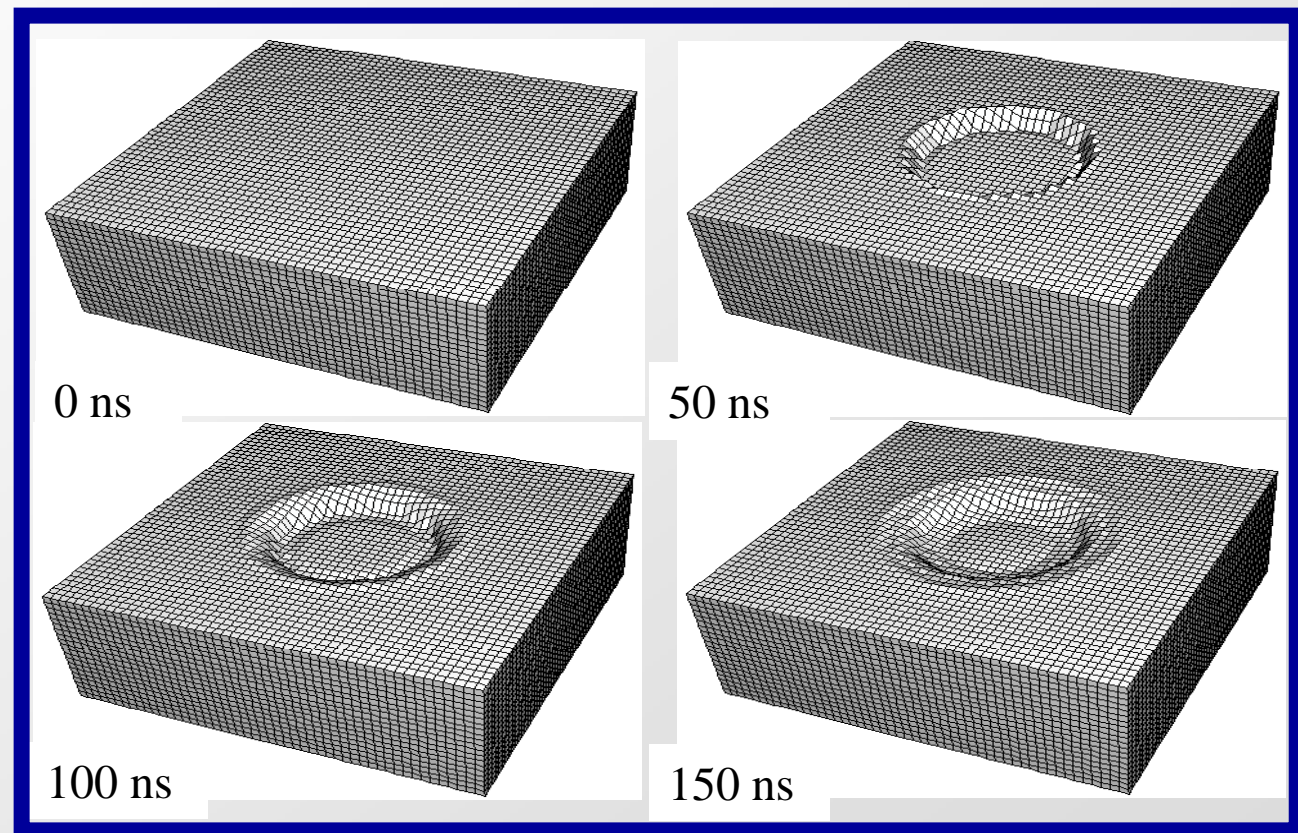
NUMERICAL SIMULATION RESULTS

HARDSHOCK-2D Semi-infinite

Ti6Al4V

Nd:YAG (1064 nm)
 $P_{av} = 5,7 \text{ W/cm}^2$
Spot radius = 0.75 mm
FWHM = 0 ns
 $\alpha = 0.15$

Multiple shocks
dynamic analysis



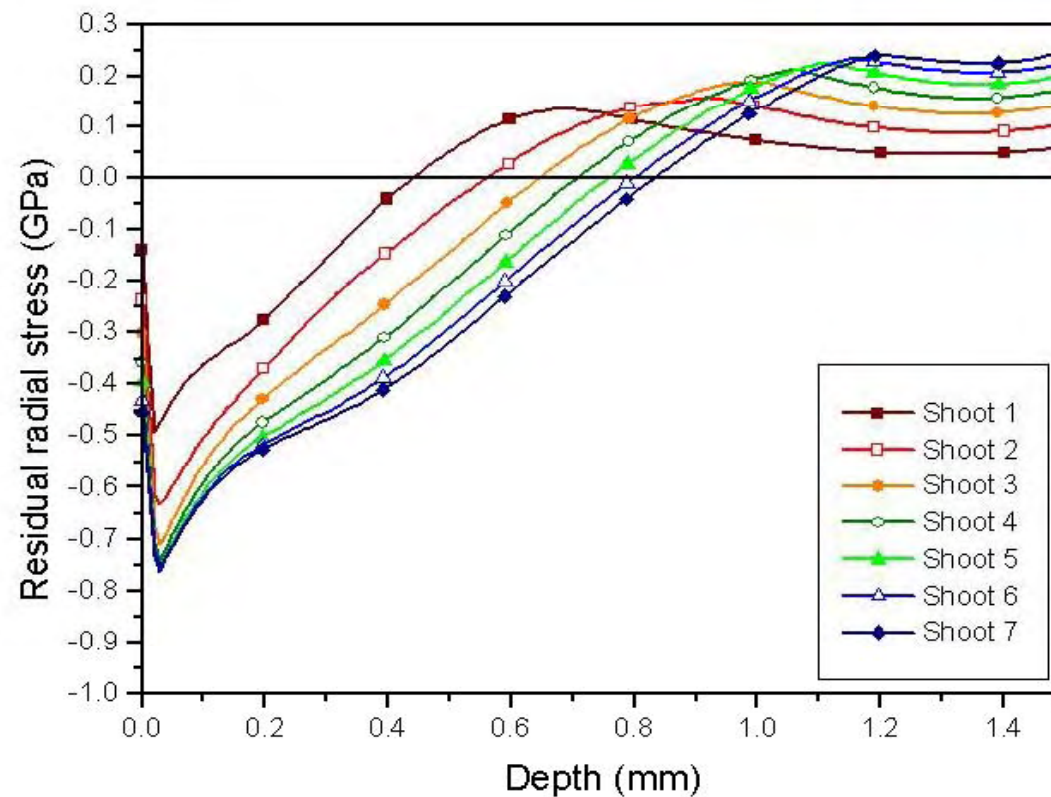
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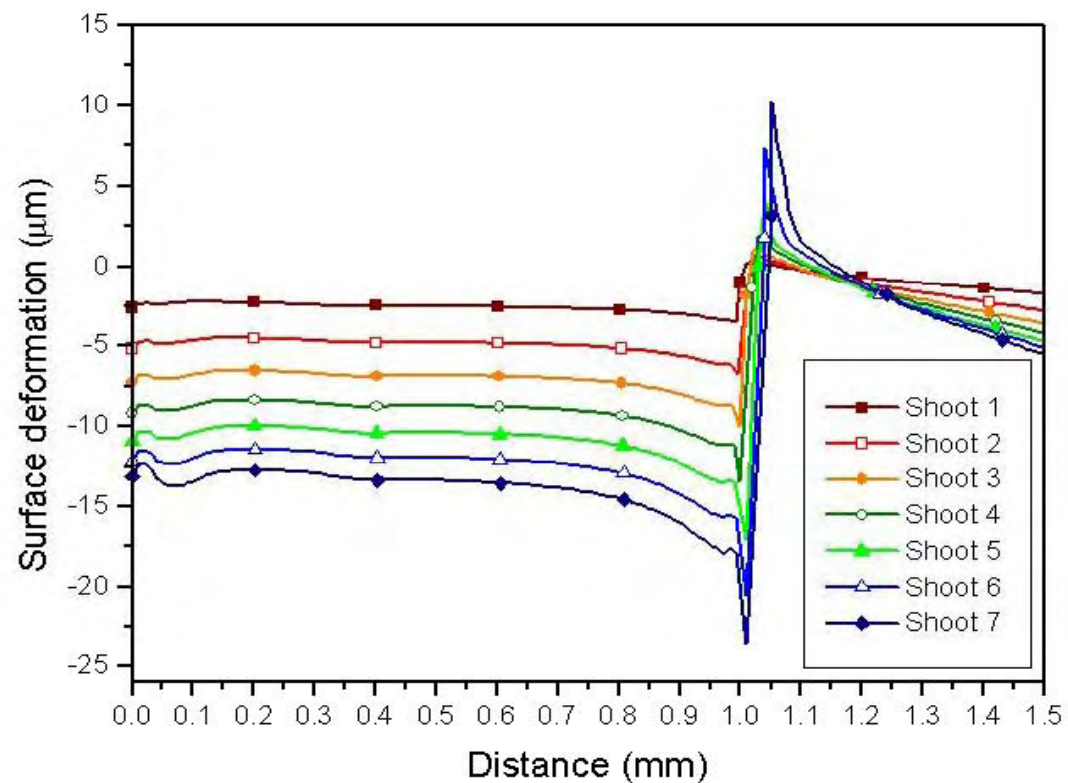
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Multiple shocks
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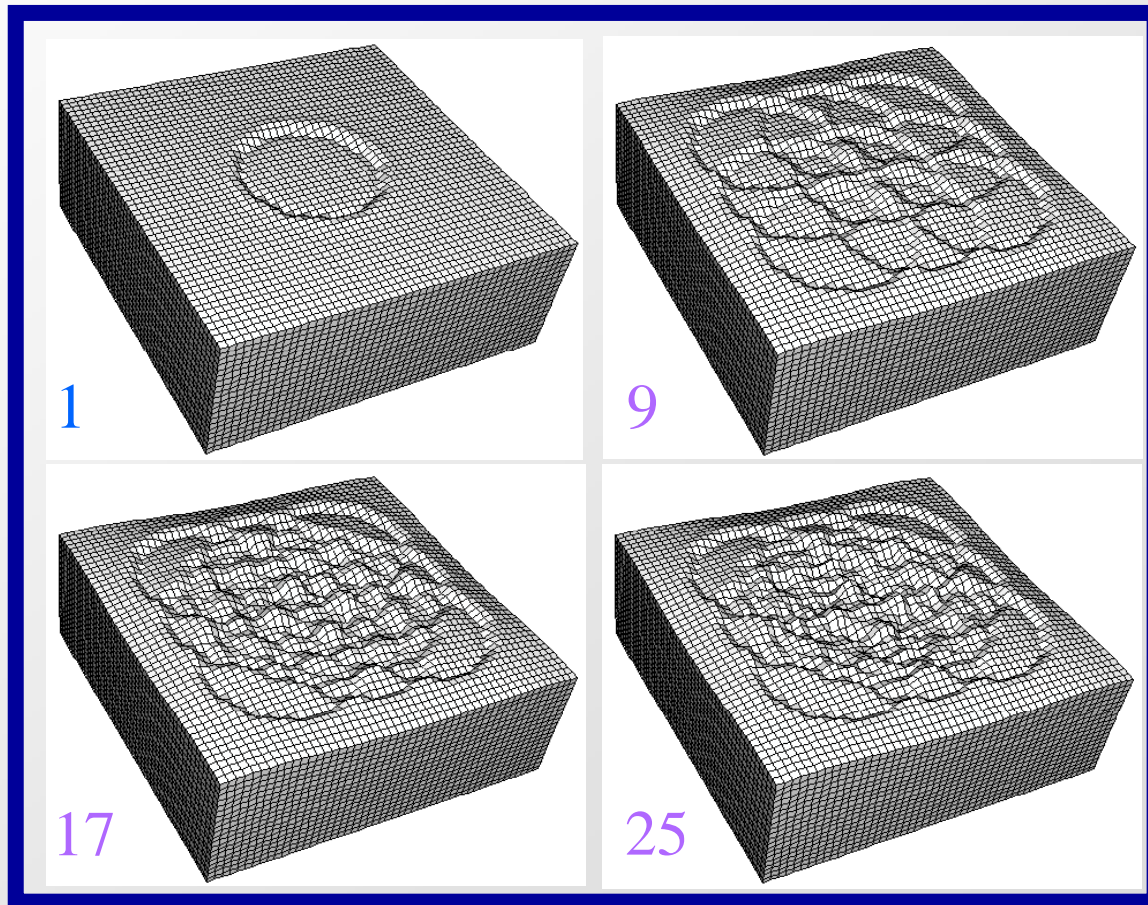


NUMERICAL SIMULATION RESULTS

HARDSHOCK-3D (full scope)

Ti6Al4V

Nd:YAG (1064 nm)
 $P_{av} = 5,7 \text{ W/cm}^2$
Spot radius = 0.75 mm
FWHM = 0 ns
 $\alpha = 0.15$
Overlapping = 900/cm²

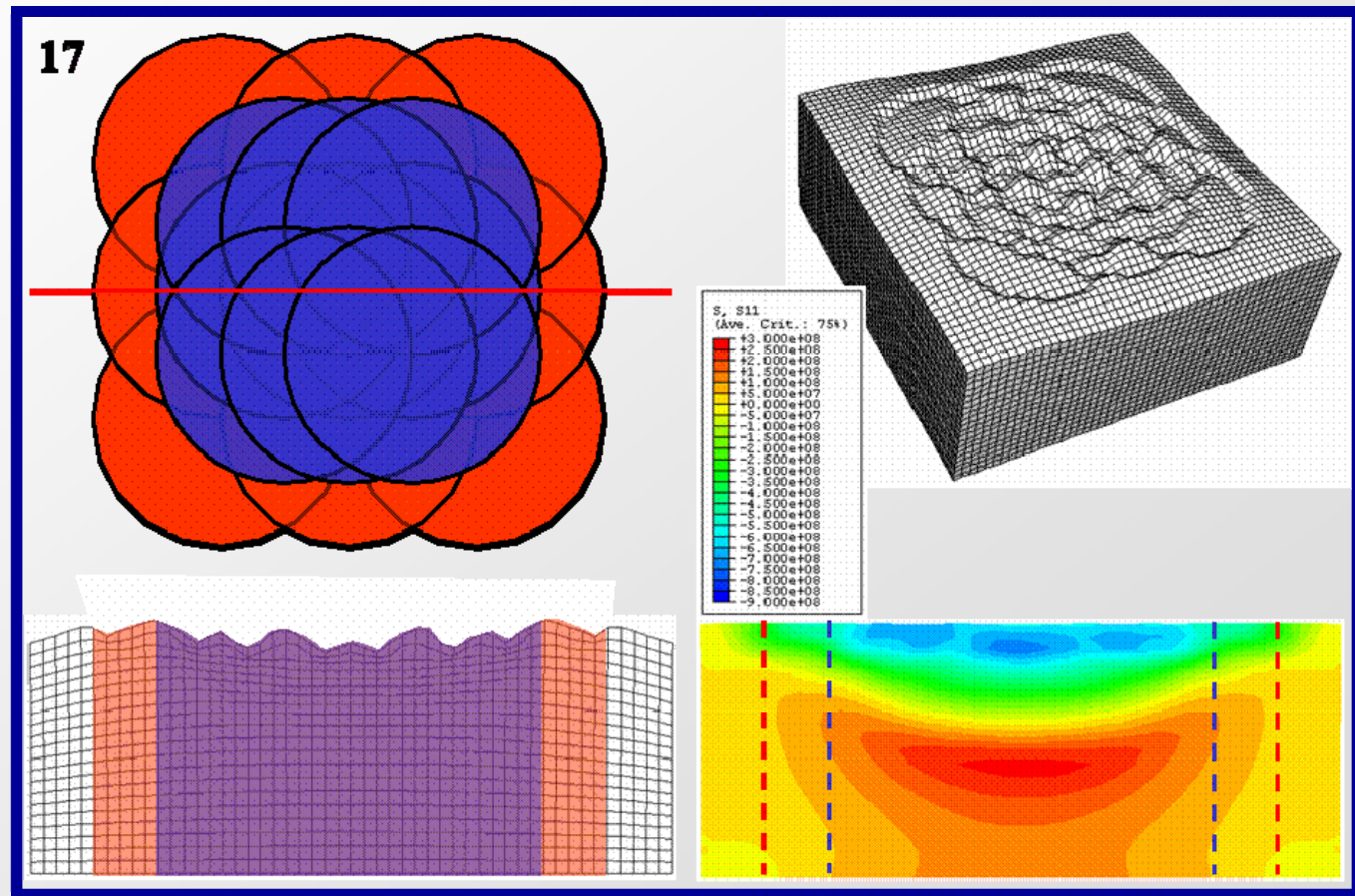


NUMERICAL SIMULATION RESULTS

HARDSHOCK-3D (full scope)

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 $P_{av} = 5,7 \text{ W/cm}^2$
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Overlapping = 900/cm²

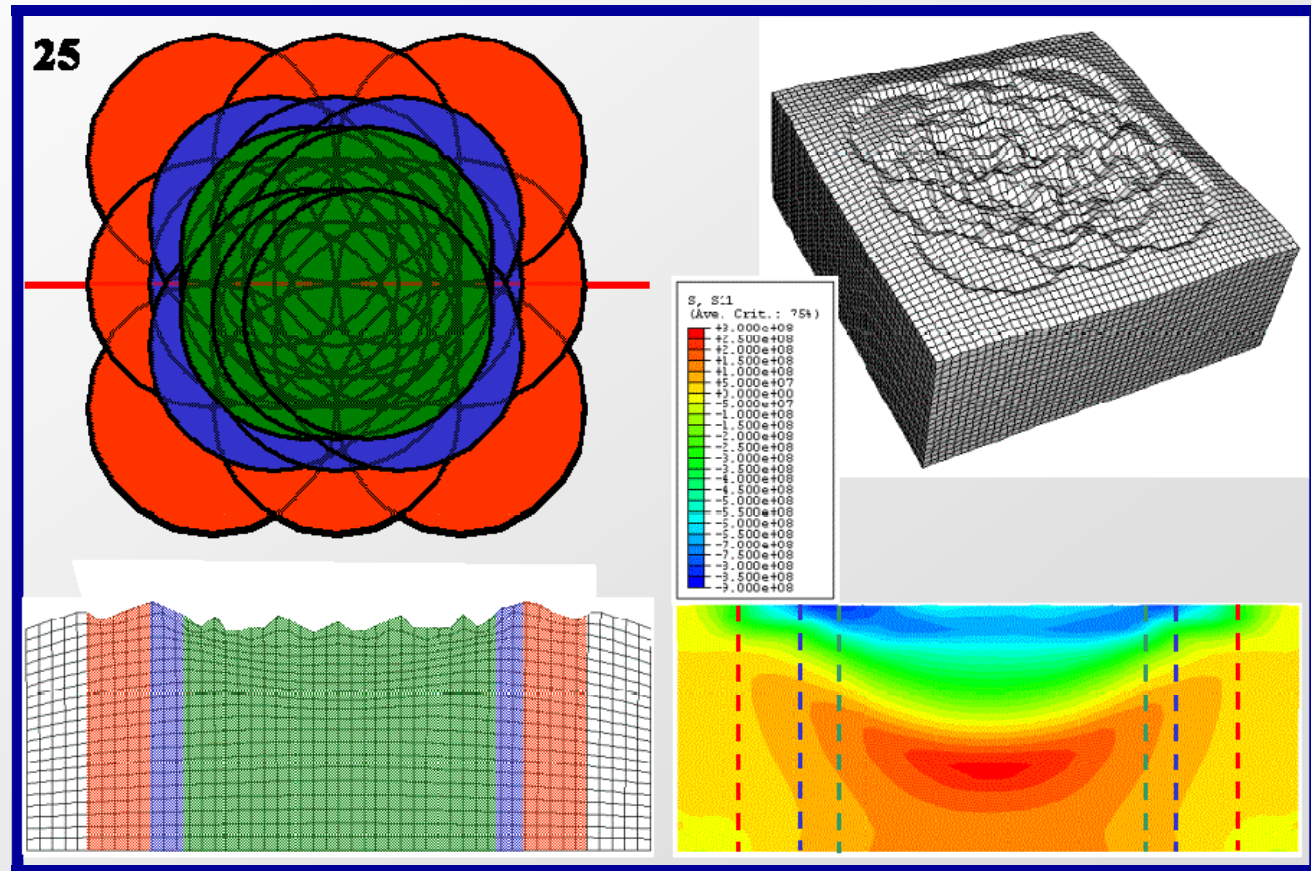


NUMERICAL SIMULATION RESULTS

HARDSHOCK-3D (full scope)

Ti6Al4V

Nd:YAG (1064 nm)
 $P_{av} = 5,7 \text{ W/cm}^2$
Spot radius = 0.75 mm
FWHM = 0 ns
 $\alpha = 0.15$
Overlapping = 900/cm²



Laser Nd:YAG ($\lambda=1064$ nm)

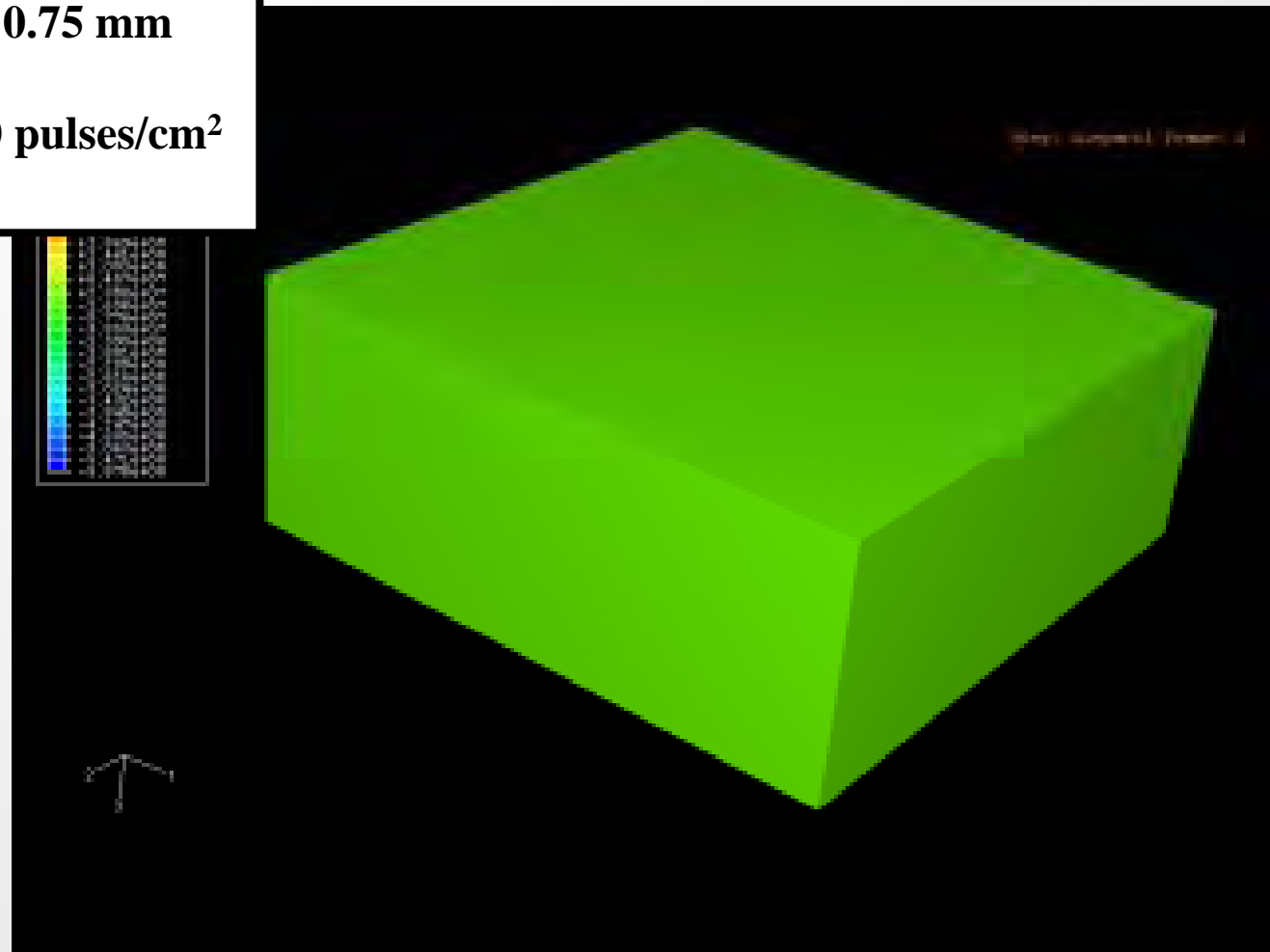
- Effective Energy 1 J
- FWHM 10 ns
- Spot radius = 0.75 mm

Material: Al2024-T3

Spot overlapping 900 pulses/cm²

$\alpha=0.15$

Residual Stress σ_x (Pa)



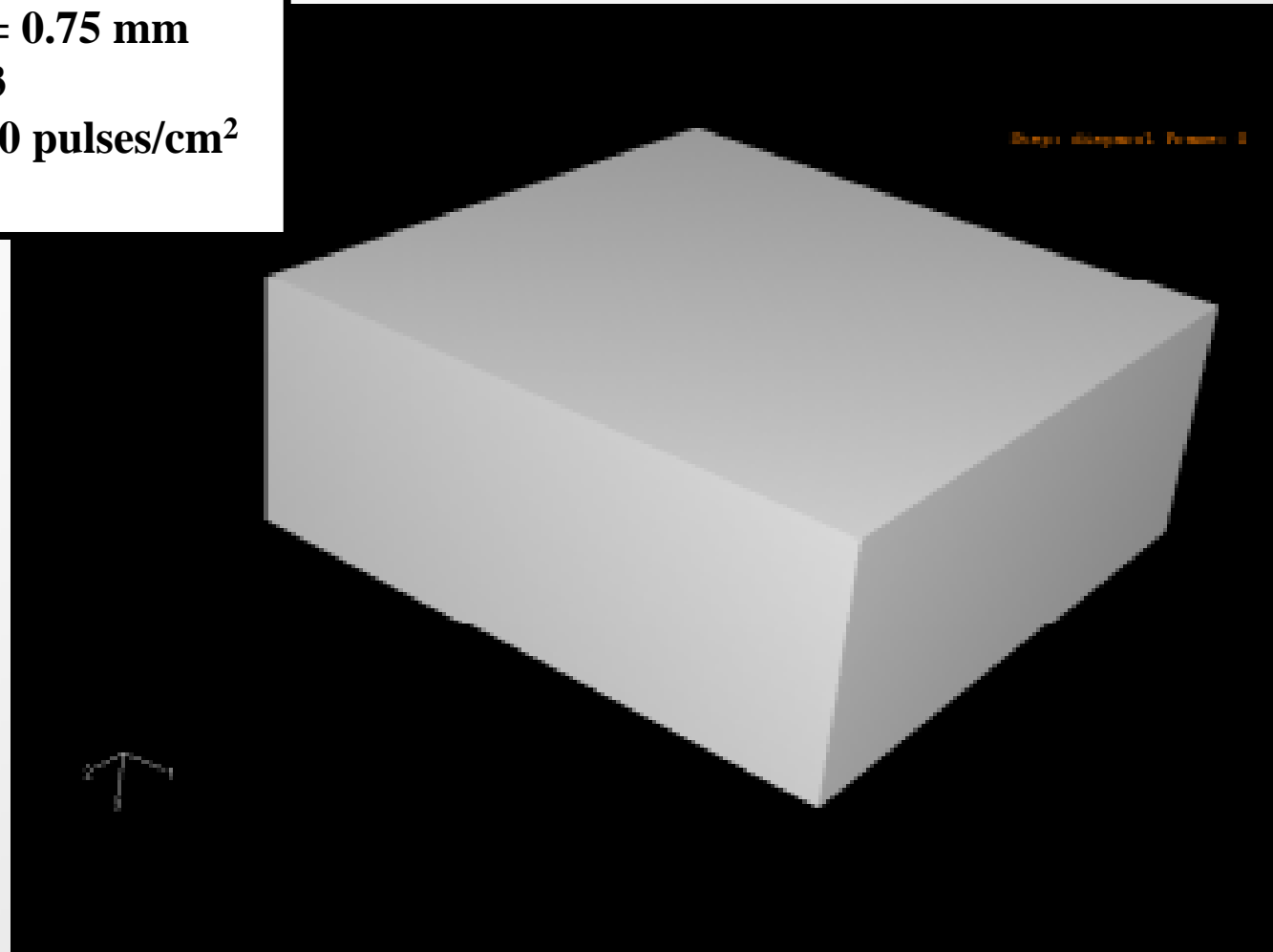
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- Effective Energy 1 J
- FWHM 10 ns
- Spot radius = 0.75 mm

Material: Al2024-T3

Spot overlapping 900 pulses/cm²
 $\alpha=0.15$

Surface deformation (x 1)



Laser Nd:YAG ($\lambda=1064$ nm)

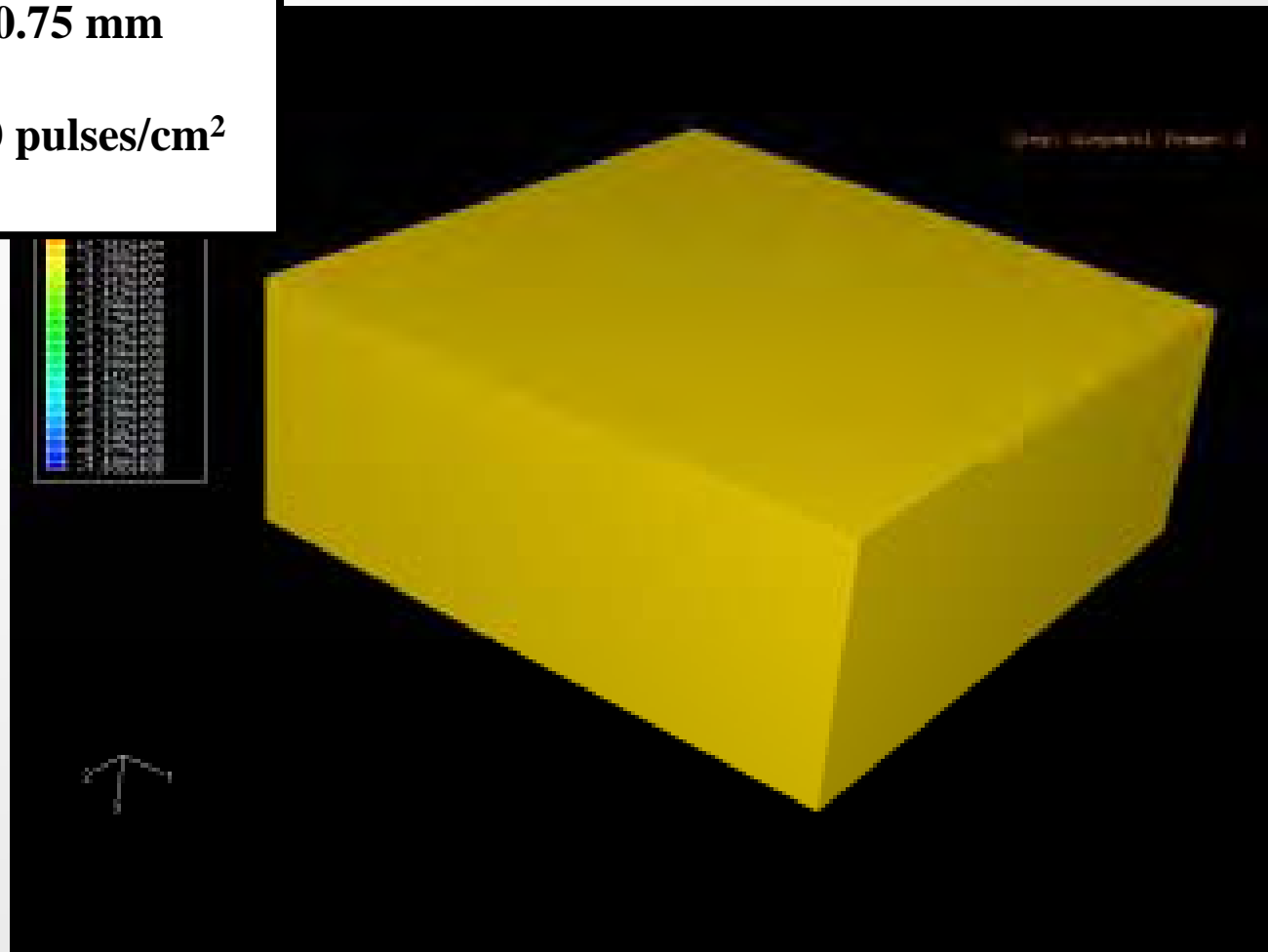
- Effective Energy 1 J
- FWHM 10 ns
- Spot radius = 0.75 mm

Material: Ti-6Al-4V

Spot overlapping 900 pulses/cm²

$\alpha = 0.15$

Residual Stress σ_x (Pa)



Laser Nd:YAG ($\lambda=1064$ nm)

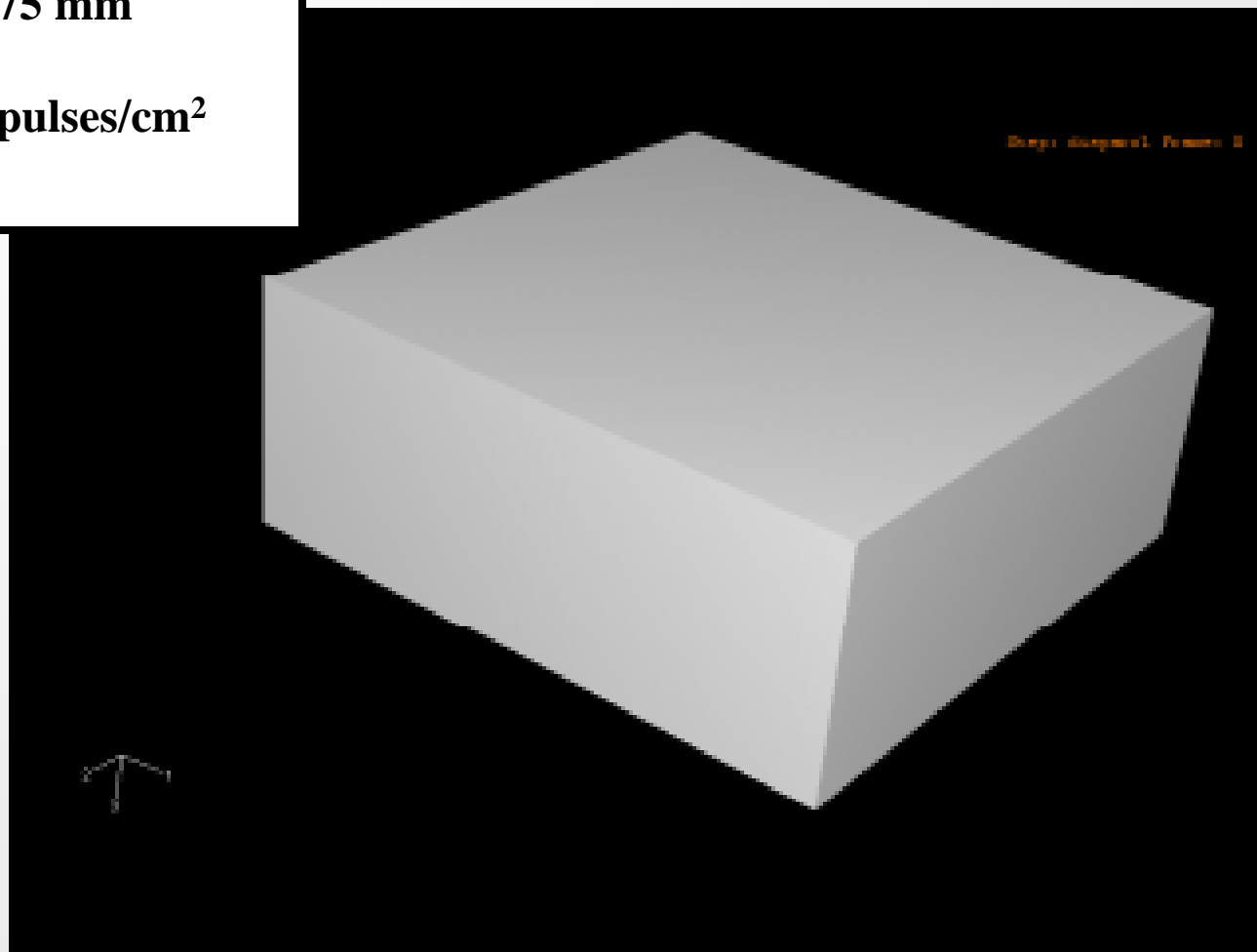
- **Effective Energy 1 J**
- **FWHM 10 ns**
- **Spot radius = 0.75 mm**

Material: Ti-6Al-4V

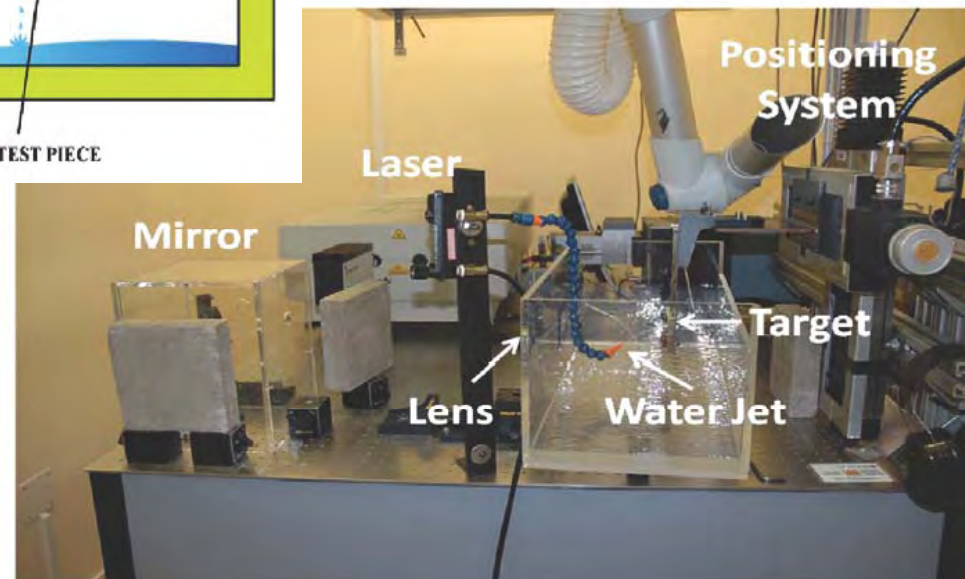
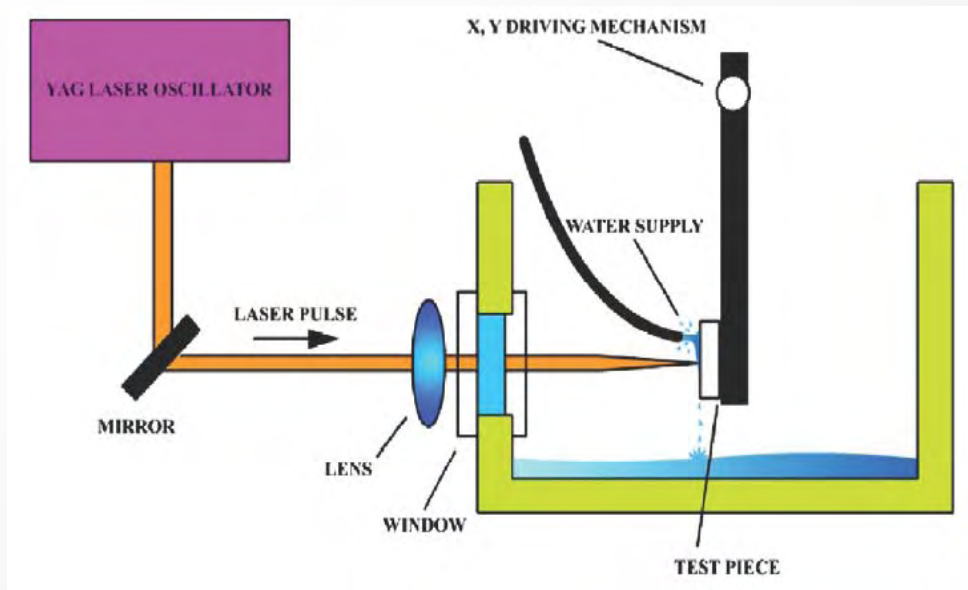
Spot overlapping 900 pulses/cm²

$\alpha=0.15$

Surface deformation (x 10)



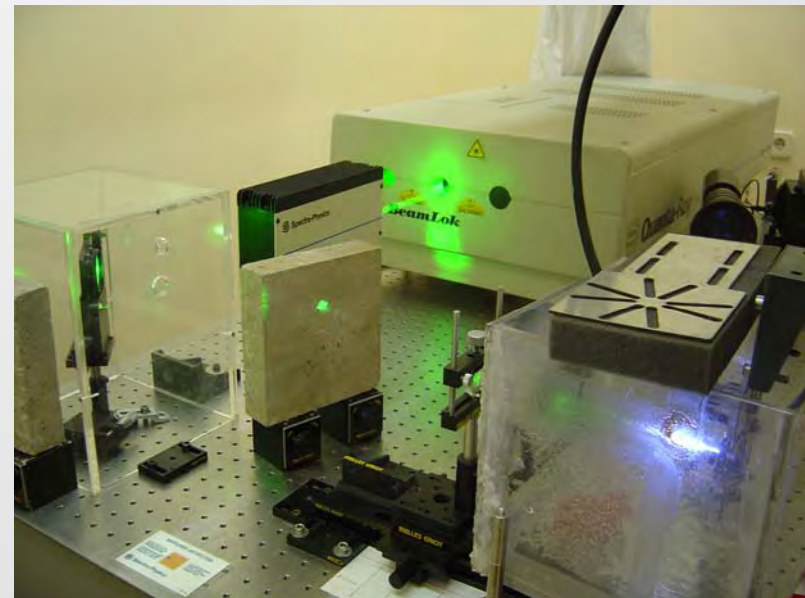
PROCESS EXPERIMENTAL SETUP



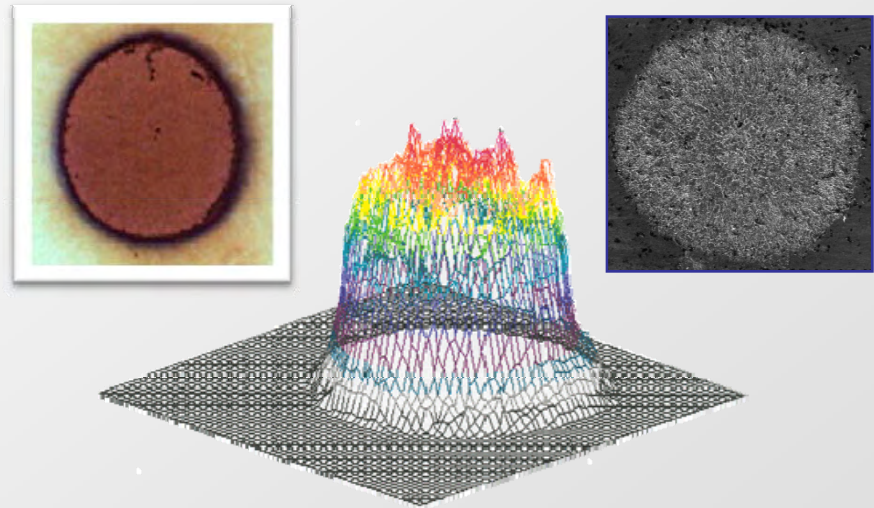
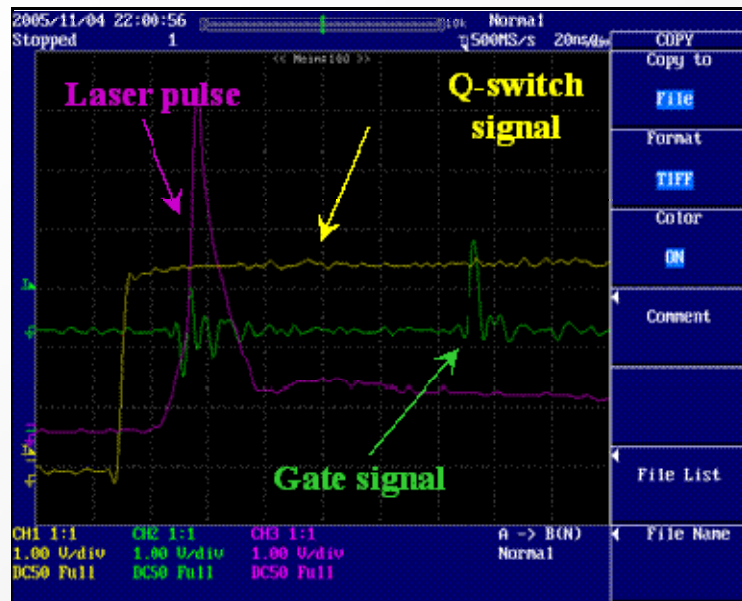
PROCESS EXPERIMENTAL SETUP

Q-SWITCHED Nd:YAG LASER

$$\left\{ \begin{array}{ll} \lambda = 1064 \text{ nm} ; E = 2,5 \text{ J/pulse} & \tau = 10 \text{ ns} ; f = 10 \text{ Hz} \\ \lambda = 532 \text{ nm} ; E = 1,4 \text{ J/pulse} \end{array} \right.$$



PROCESS EXPERIMENTAL SETUP



LSP TREATMENT PARAMETERS

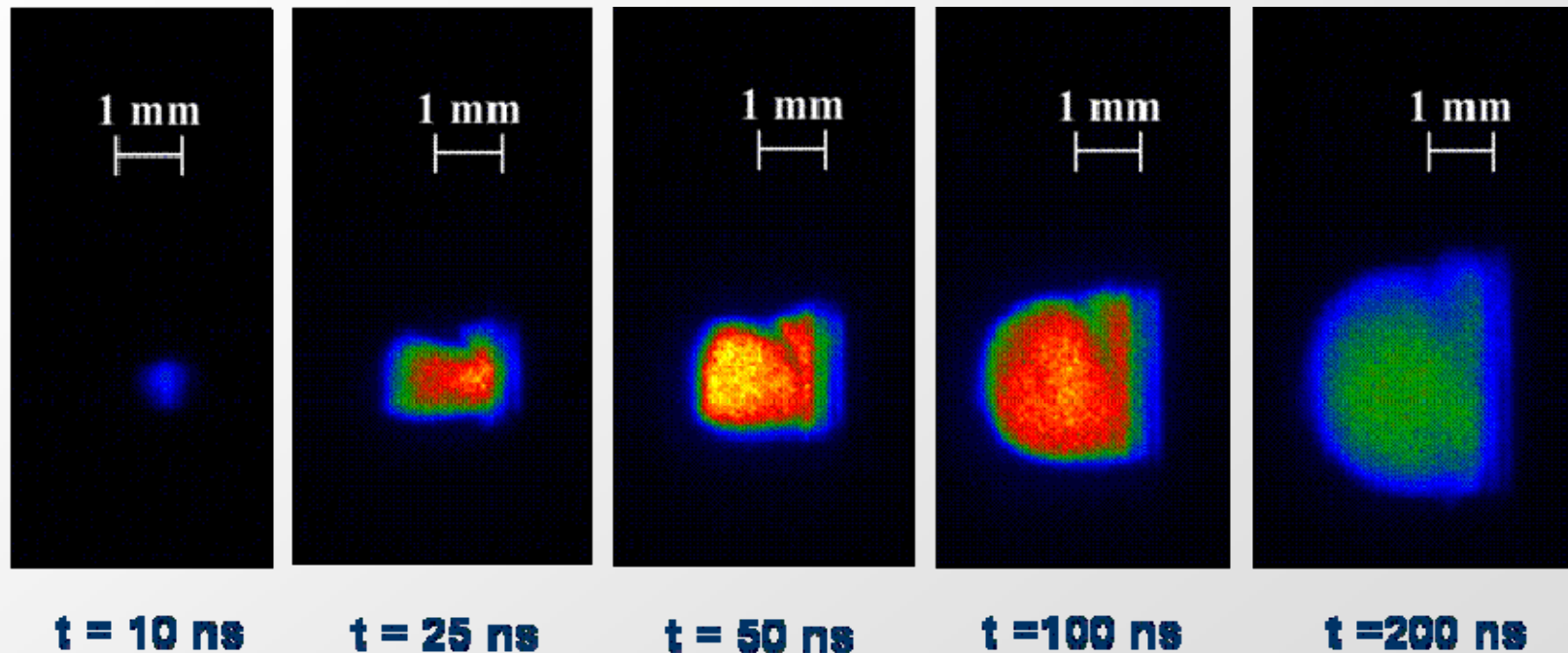
Laser wavelength (nm) ; Q-switched Nd:YAG	1064
Energy per pulse (J/pulse)	2,0
Pulse temporal width (ns)	≈ 9
Laser spot diameter (mm)	1.5
Ratio x-y pitch	1
Confining medium	Water jet ≈ 2 bar
Absorbing coating overlay	No

PROCESS EXPERIMENTAL SETUP



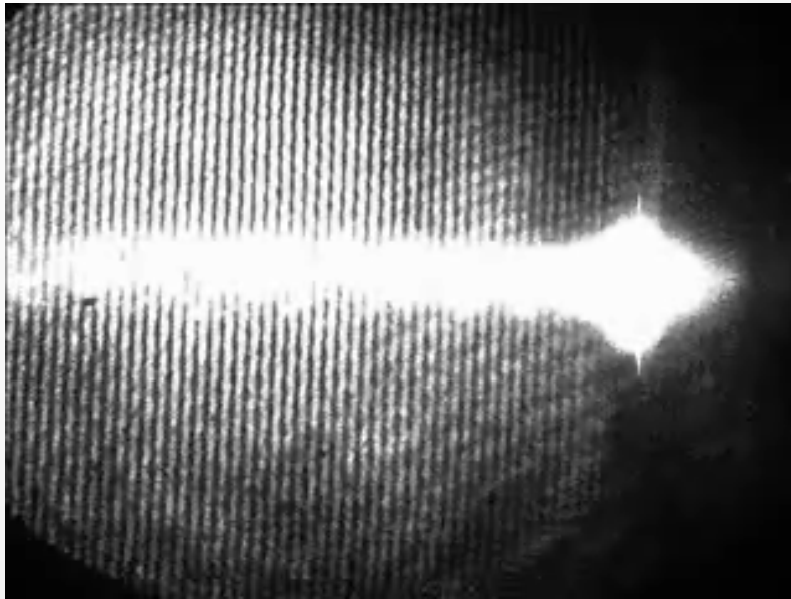
EXPERIMENTAL VALIDATION. DIAGNOSIS SETUP

DIRECT IMAGING - HYDRODYNAMIC ANALYSIS

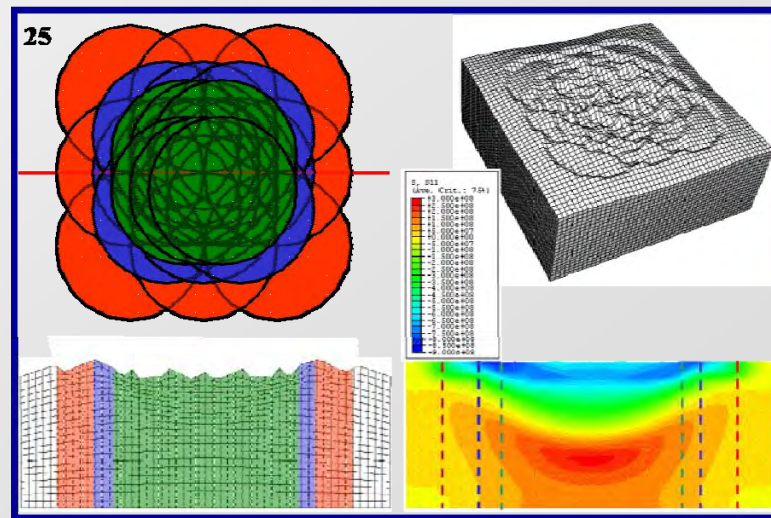
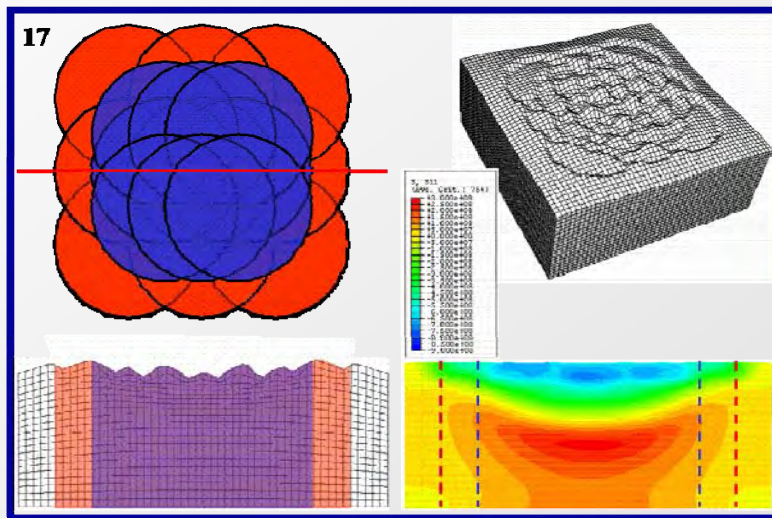
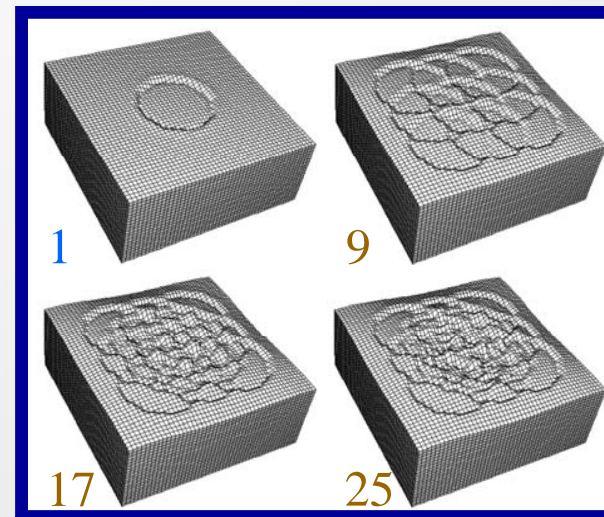
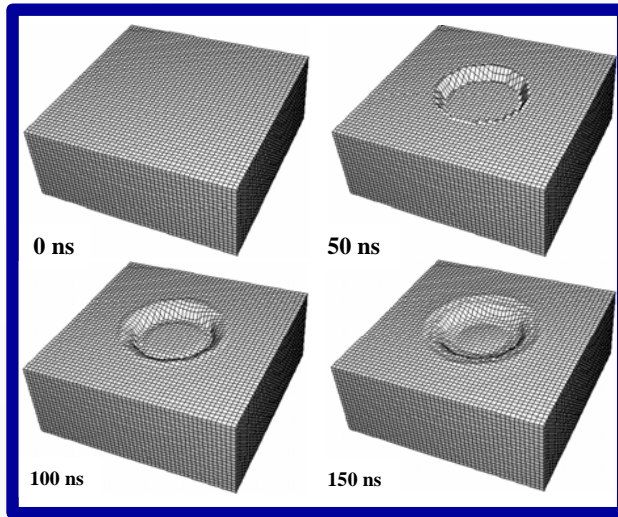


EXPERIMENTAL VALIDATION. DIAGNOSIS SETUP

IMAGING TECHNIQUES – SCHLIEREN / INTERFEROMETRY



EXPERIMENTAL PROCEDURE



EXPERIMENTAL PROCEDURE

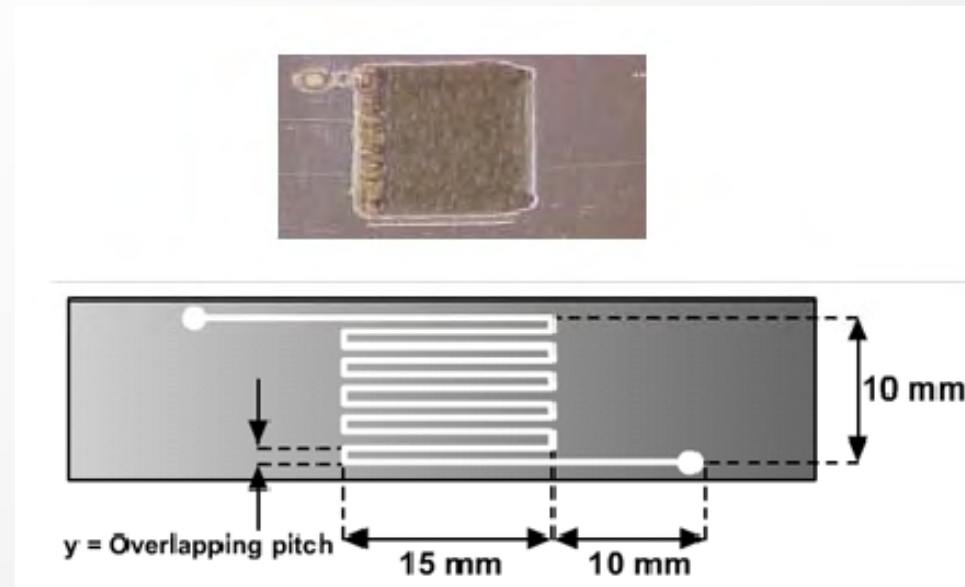
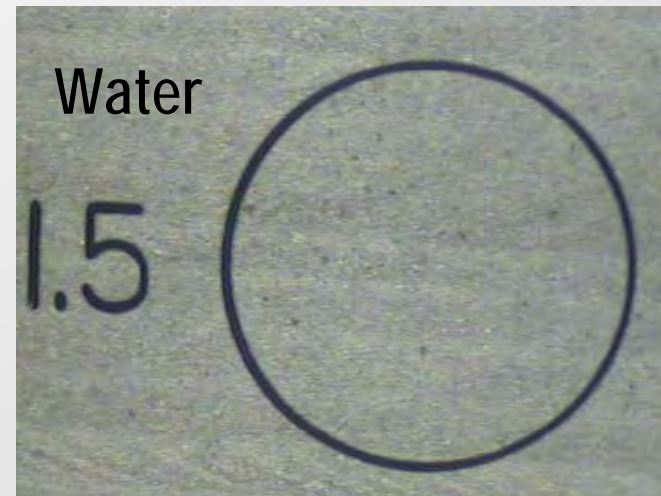
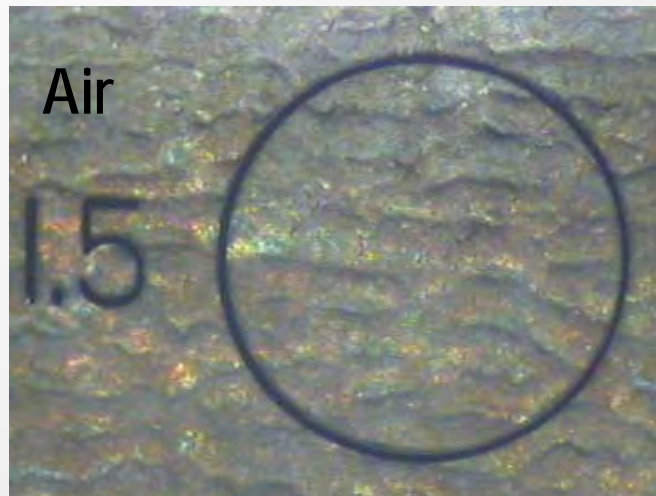


Table I: Relation between overlapping pitch and equivalent number of pulses per unit surface corresponding to the defined sweeping procedure.

Overlapping pitch Y (mm)	Equivalent overlapping density (pulses/cm ²)
0.588	289
0.33	900
0.285	1225
0.2	2500
0.141	5000

EXPERIMENTAL RESULTS

Material: Al2024 T3
Pulses: $\varnothing=1,5$ mm; $\tau=10$ ns; $f=10$ Hz;
 $E=1$ J/pulse; $I=1,41$ GW/cm²
Swept Area : 15x15 mm²; 2500 pulses/cm²



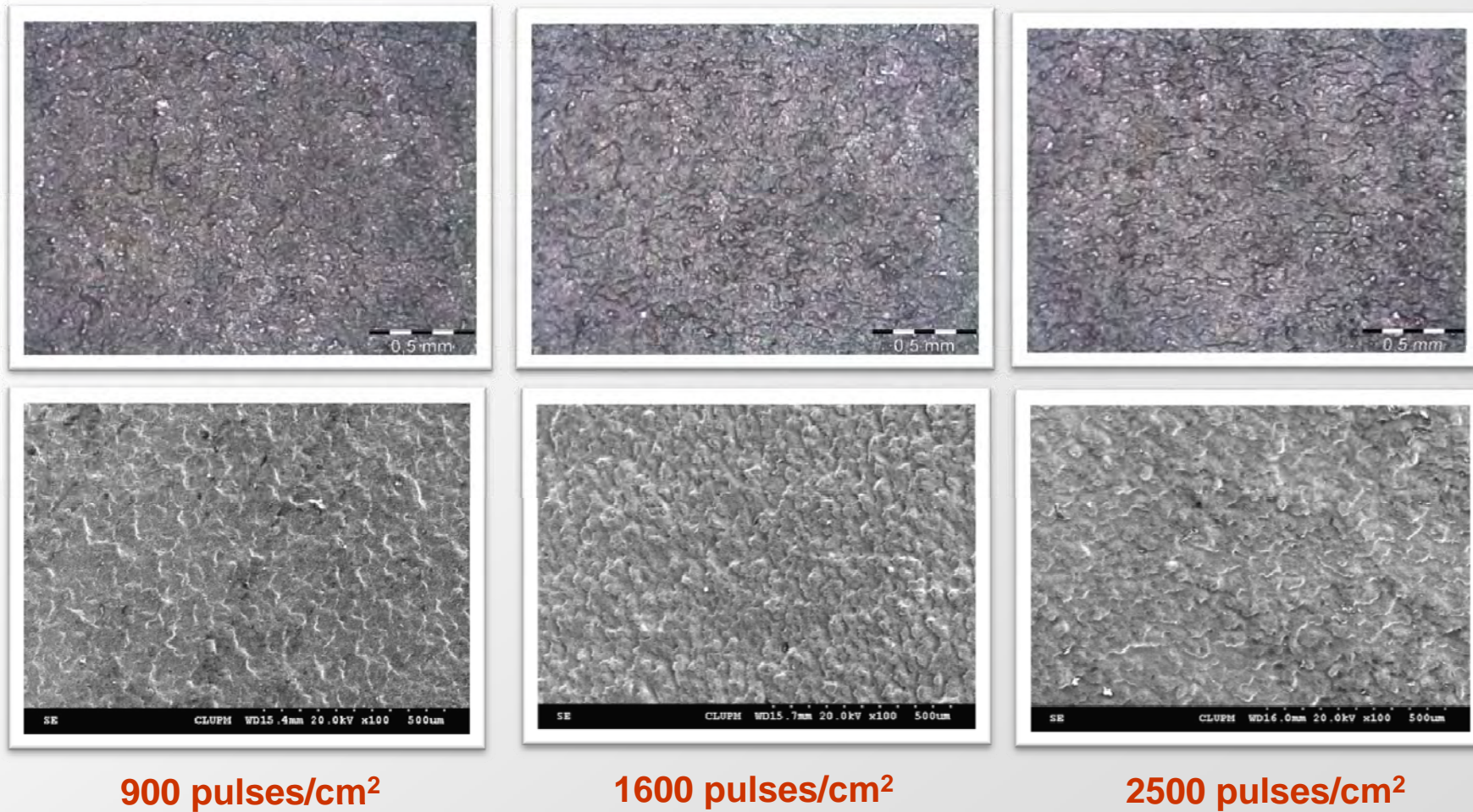
EXPERIMENTAL RESULTS

Reported Analysis

	Al2024-T351 30x20x8 mm ³	Ti6Al4V 30x20x10 mm ³
900 pulses/cm ²		
1600 pulses/cm ²		
2500 pulses/cm ²		
5000 pulses/cm ²		

EXPERIMENTAL RESULTS

Surface Roughness (Microscopy): Al2024-T351



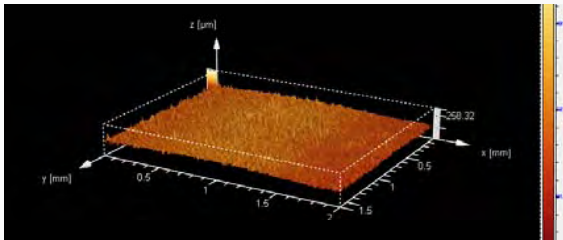
900 pulses/cm²

1600 pulses/cm²

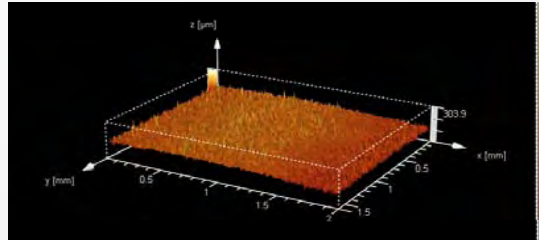
2500 pulses/cm²

EXPERIMENTAL RESULTS

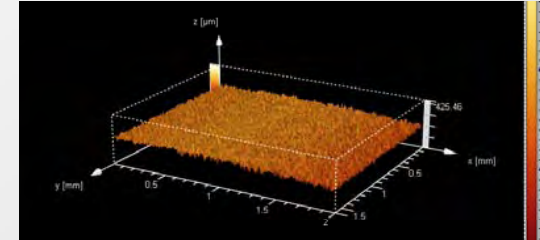
Surface Roughness (Topographic Confocal microscopy): Al2024-T351



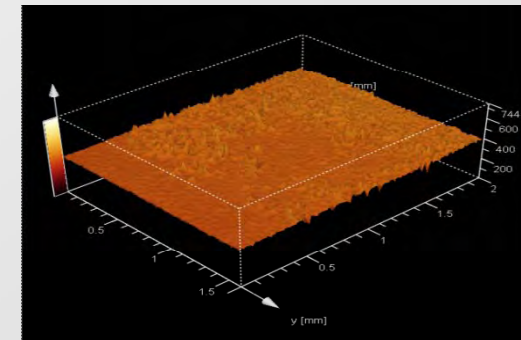
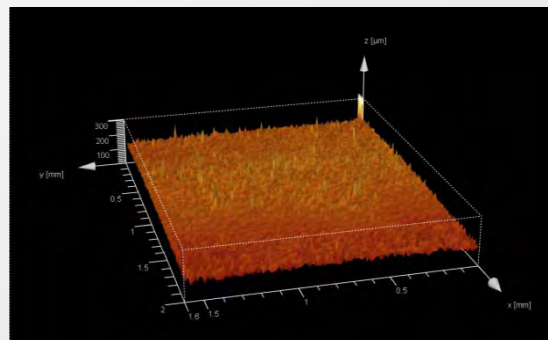
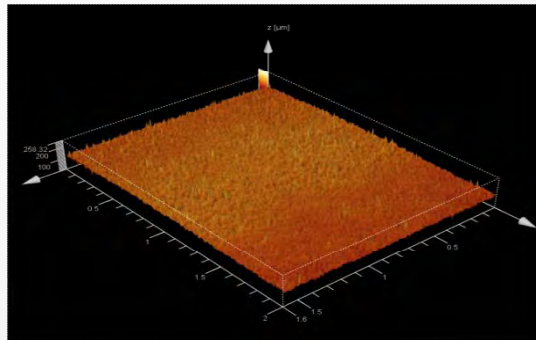
900 pulses/cm²



1600 pulses/cm²



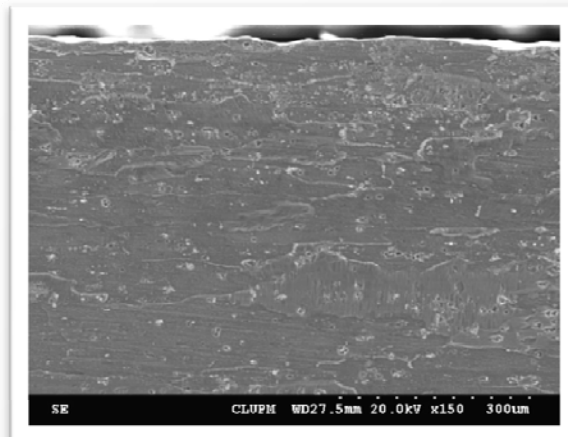
2500 pulses/cm²



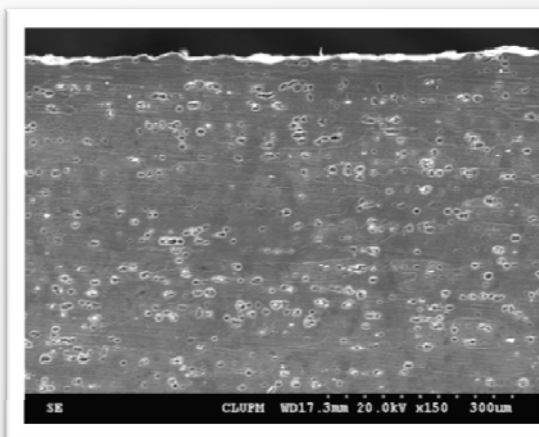
	No treatment	900 pulses/cm ²	1600 pulses/cm ²	2500 pulses/cm ²
Pa (μm)	7.96	5.23	4.82	4.96
<Δz>	----	10.30	20.00	26.82

EXPERIMENTAL RESULTS

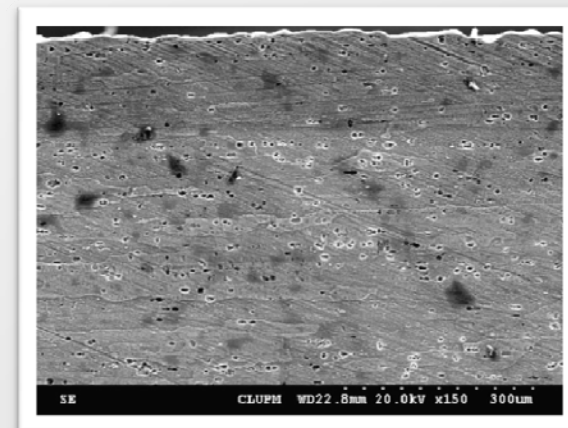
Microscopic material compactation: Al2024-T351



900 pulses/cm²



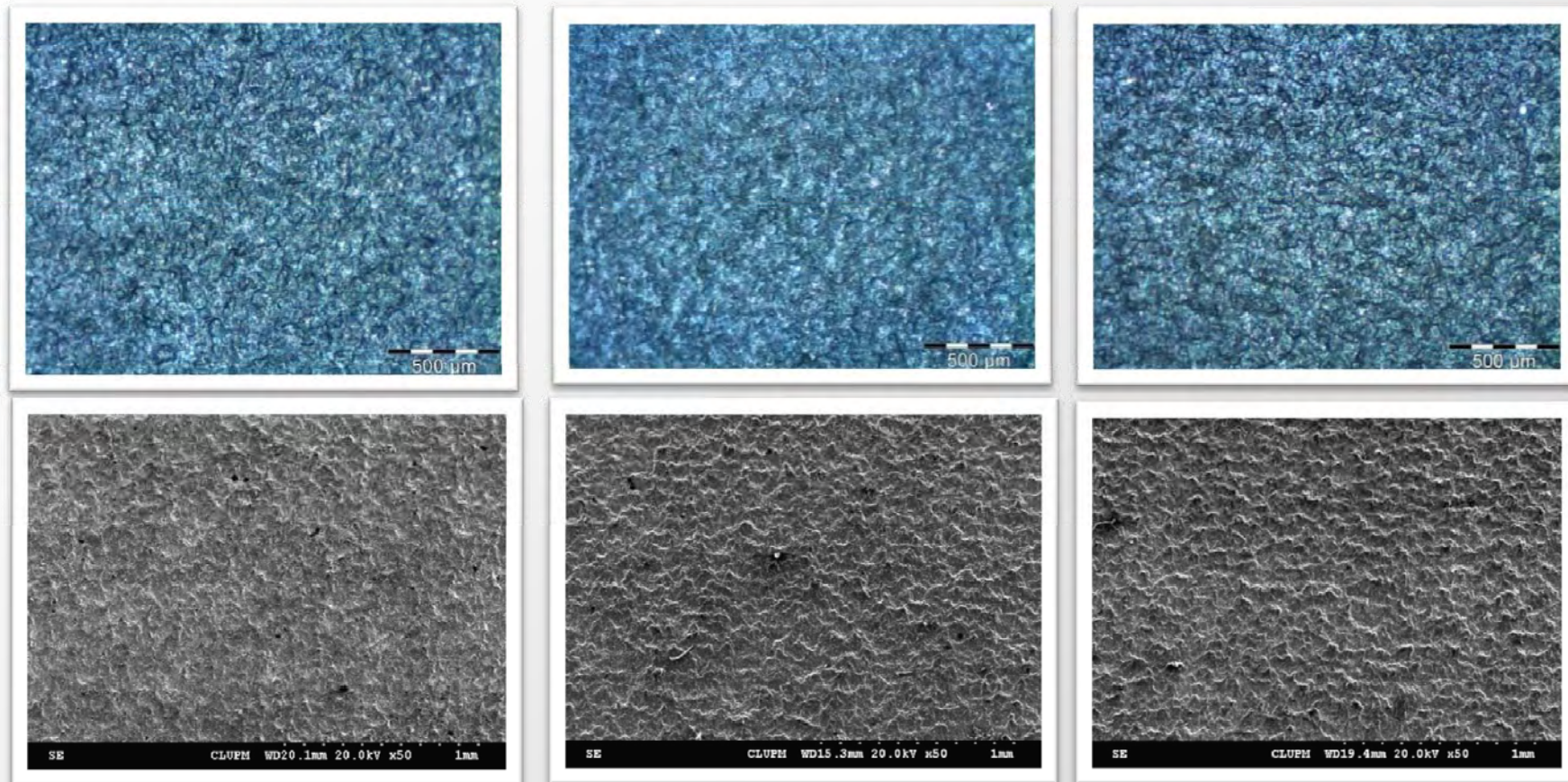
1600 pulses/cm²



2500 pulses/cm²

EXPERIMENTAL RESULTS

Surface Roughness (Microscopy): Ti6Al4V



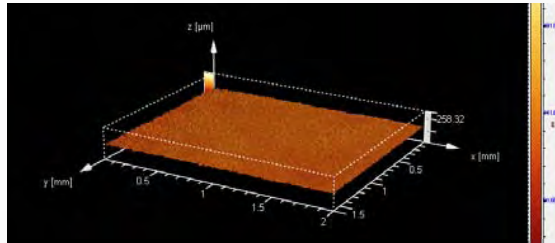
900 pulses/cm²

2500 pulses/cm²

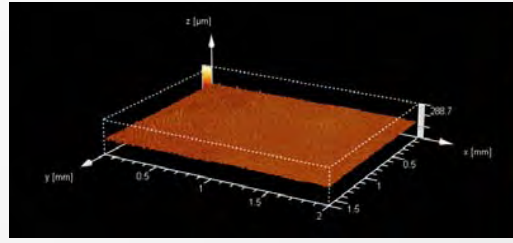
5000 pulses/cm²

EXPERIMENTAL RESULTS

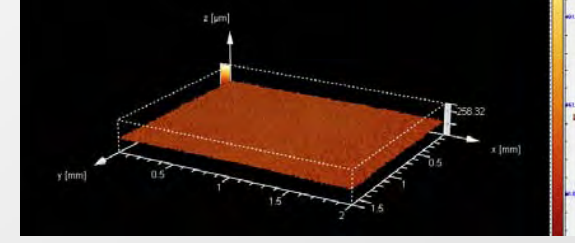
Surface Roughness (Topographic Confocal microscopy): Ti6Al4V



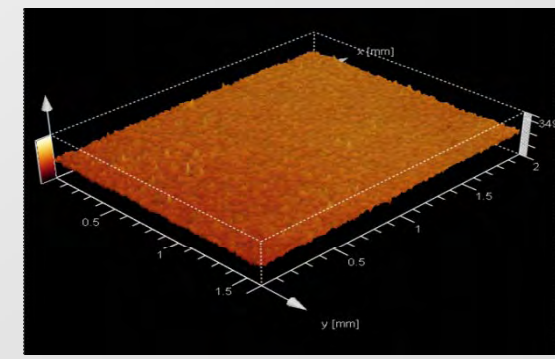
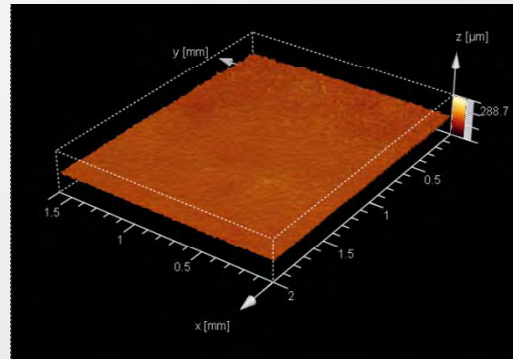
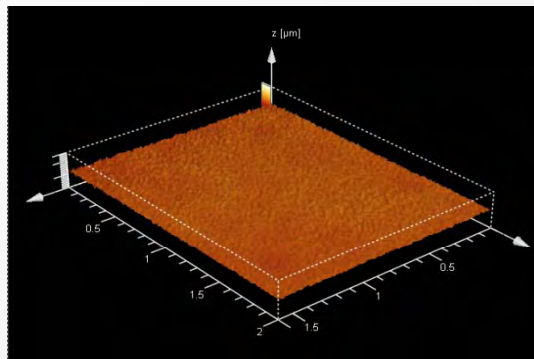
900 pulses/cm²



2500 pulses/cm²



5000 pulses/cm²



	No treatment	900 pulses/cm ²	1600 pulses/cm ²	2500 pulses/cm ²
Pa (μm)	9.98	3.62	3.87	3.87
<Δz>	---	2.81	7.40	5.80

EXPERIMENTAL RESULTS

Microscopic material compactation: Ti6Al4V



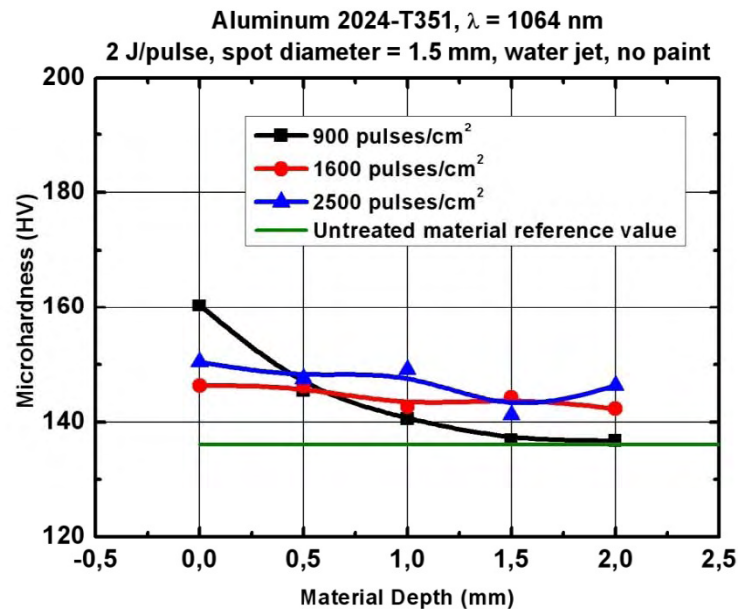
900 pulses/cm²

2500 pulses/cm²

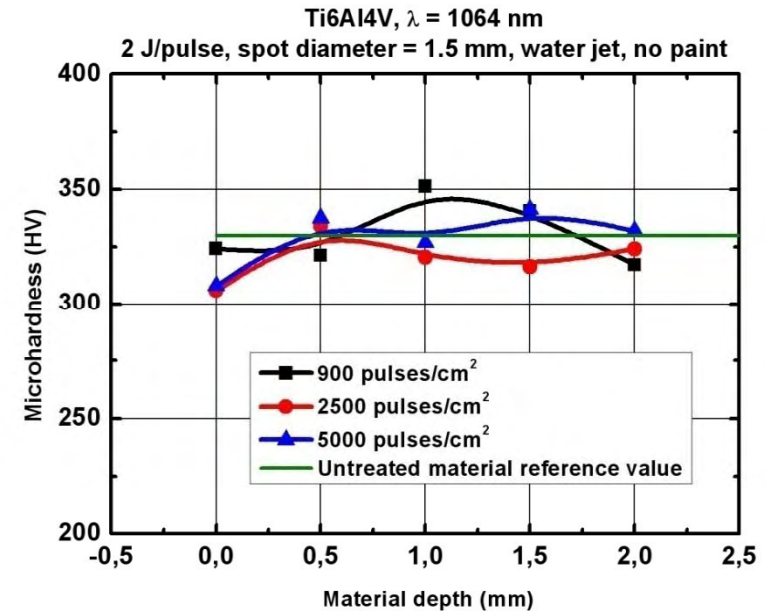
5000 pulses/cm²

EXPERIMENTAL RESULTS

Microhardness (HV)



Slight increase in microhardness in Al2024-T351
Higher for higher LSP treatment intensity

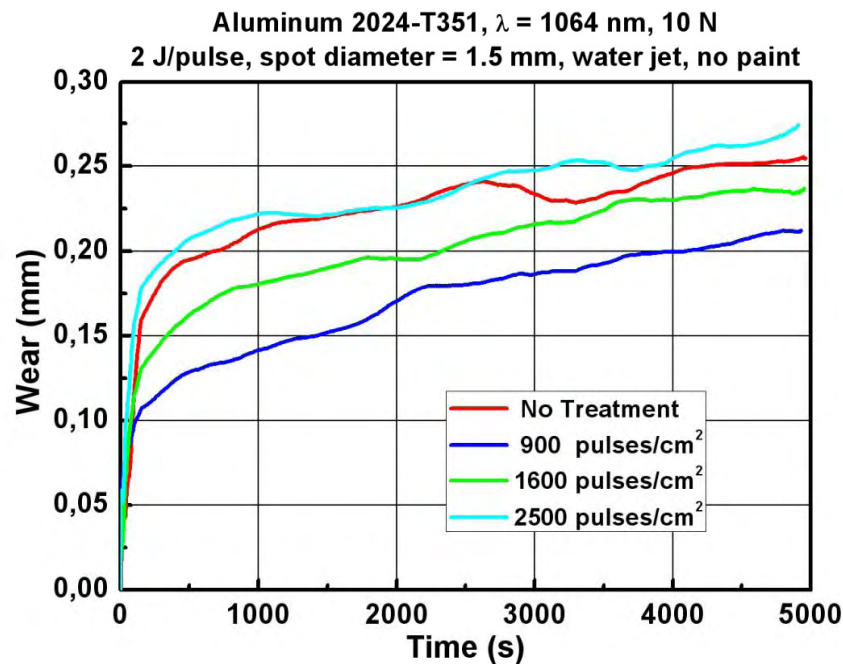


No apparent hardening effect in Ti6Al4V.

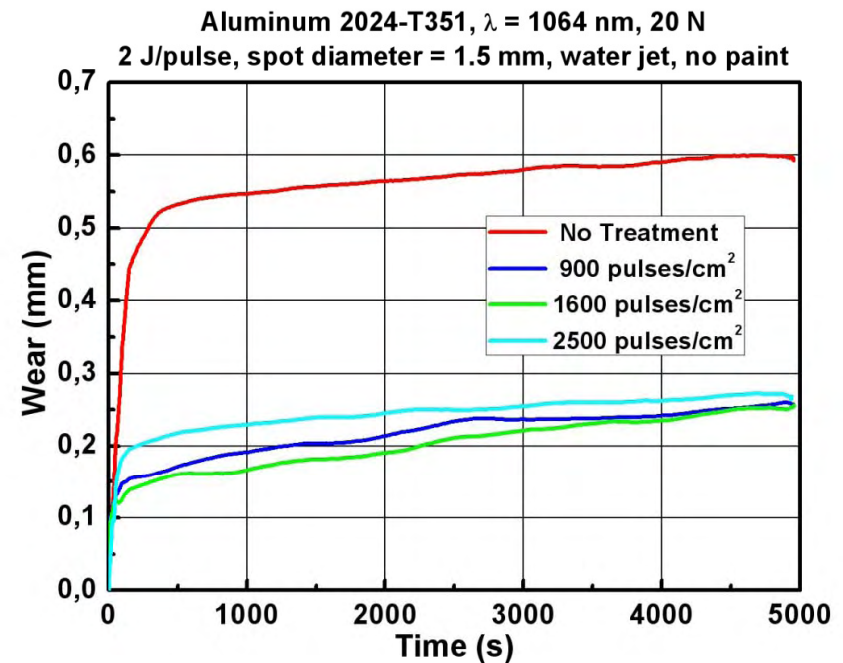
EXPERIMENTAL RESULTS

Wear resistance (According to ASTM G99-04)

Al2024-T351



Slight wear improvement in
Al2024-T351 at low loads

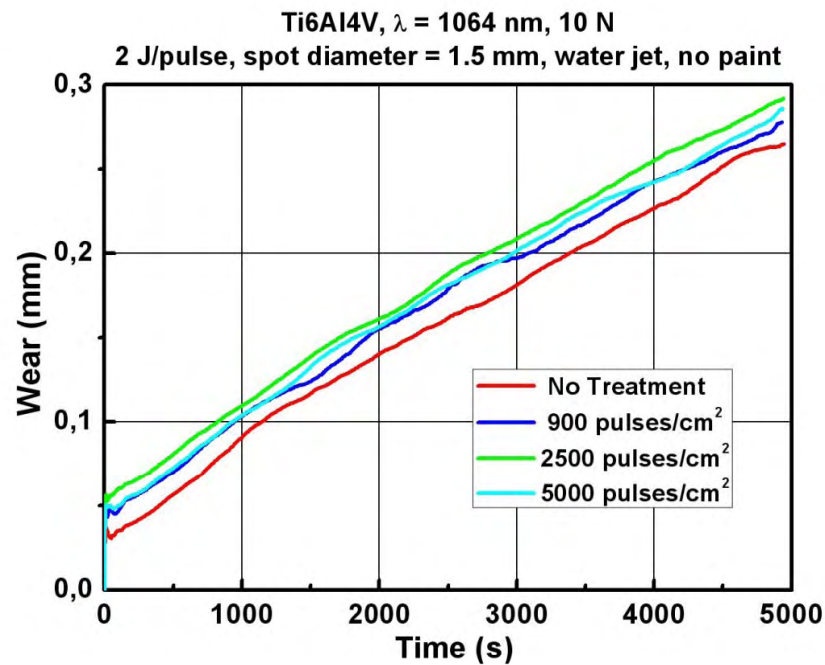


Considerable wear improvement in
Al2024-T351 at moderate loads

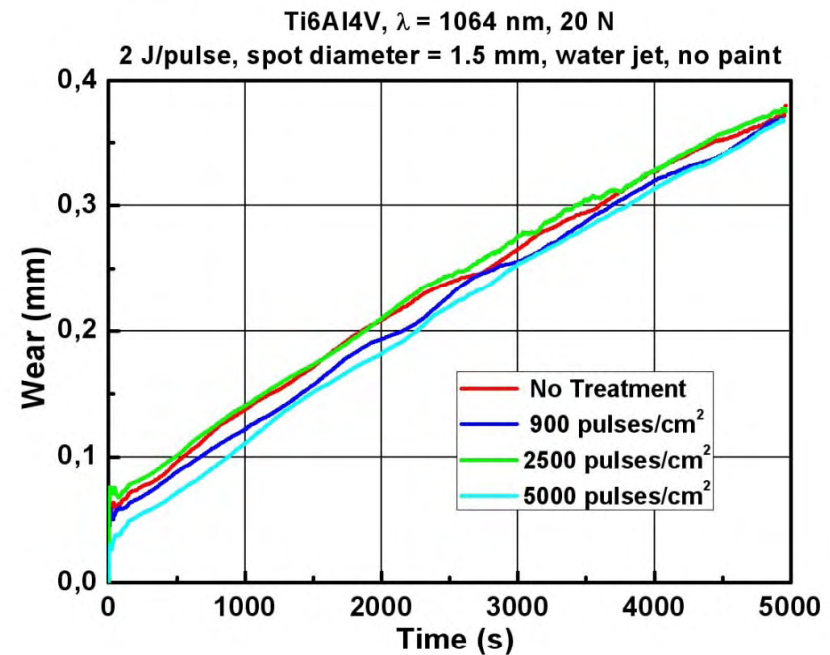
EXPERIMENTAL RESULTS

Wear resistance (According to ASTM G99-04)

Ti6Al4V



Slight negative wear impact in
Ti6Al4V at low loads

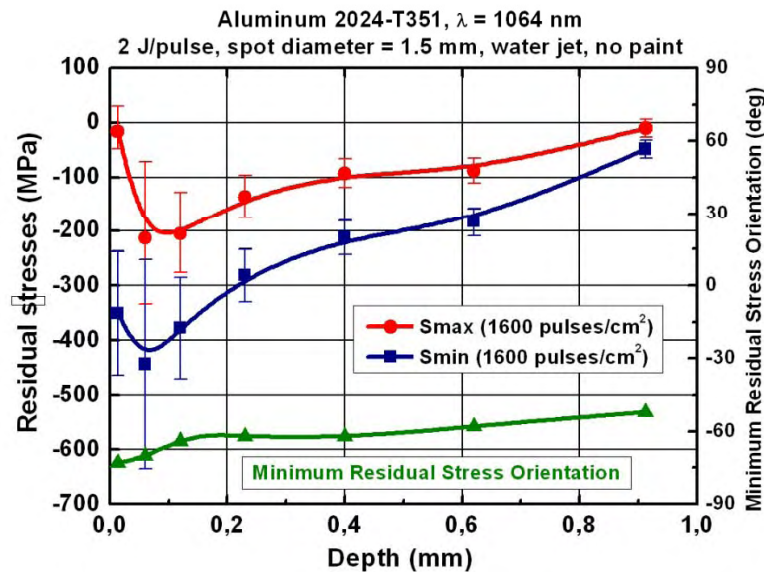


Inappreciable wear improvement in
Ti6Al4V at moderate loads

EXPERIMENTAL RESULTS

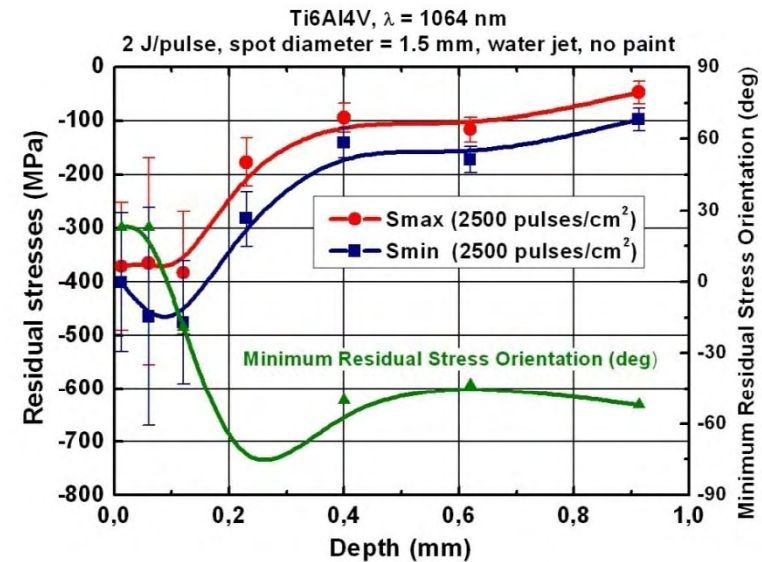
Residual Stresses (According to ASTM E837-08)

Al2024-T351



Relatively broad difference between S_{max} and S_{min} in Al2024-T351

Ti6Al4V

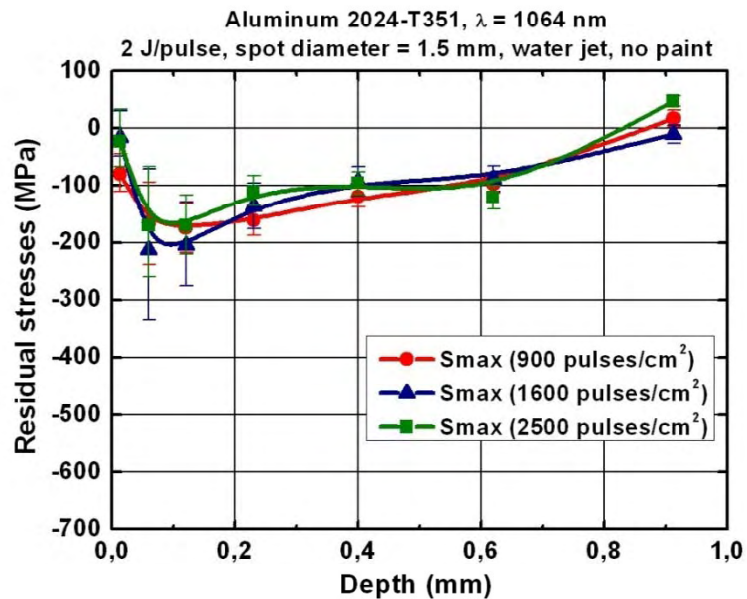


Relatively small difference between S_{max} and S_{min} in Ti6Al4V

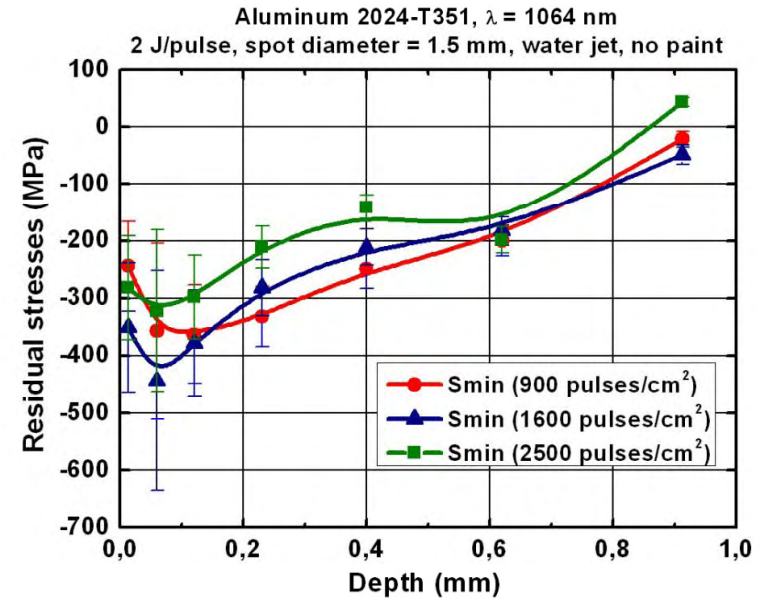
EXPERIMENTAL RESULTS

Residual Stresses (According to ASTM E837-08)

Al2024-T351



S_{max} in Al2024-T351 for different irradiation intensities

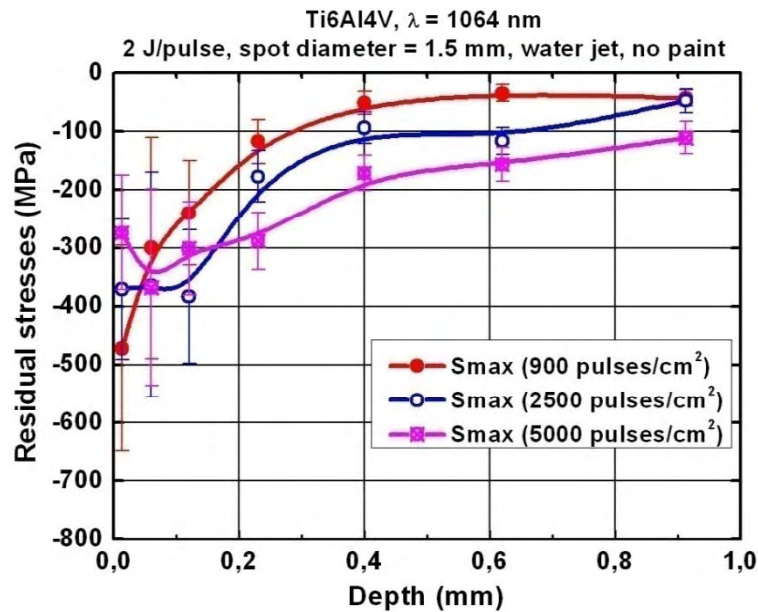


S_{min} in Al2024-T351 for different irradiation intensities

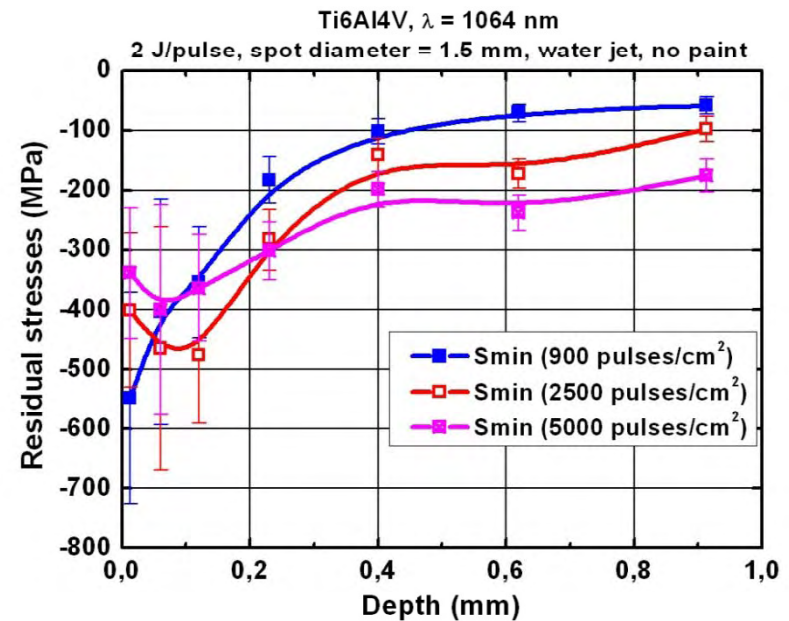
EXPERIMENTAL RESULTS

Residual Stresses (According to ASTM E837-08)

Ti6Al4V

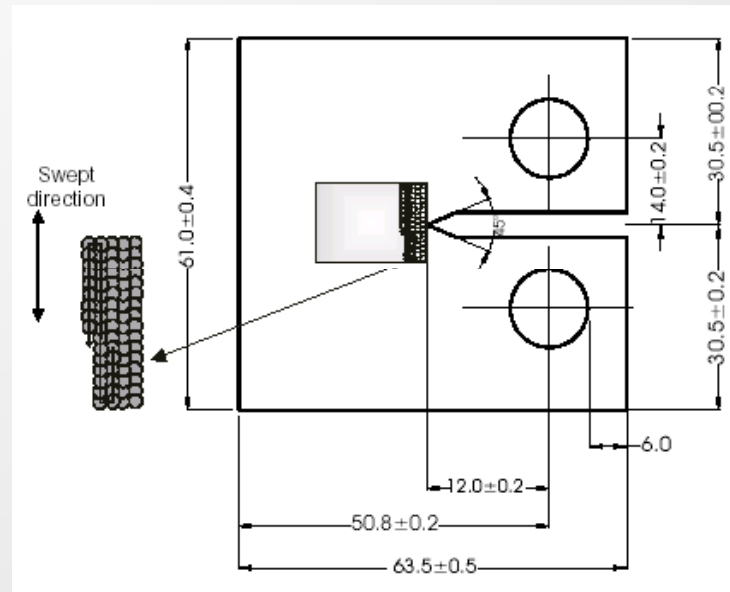
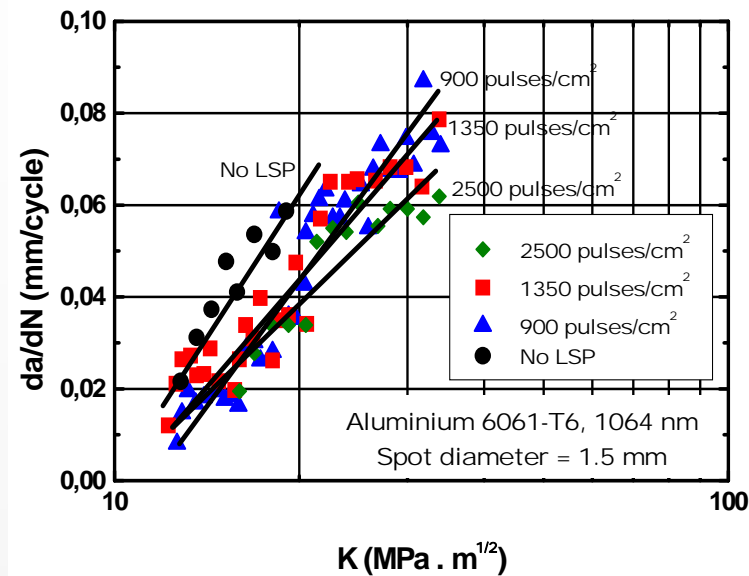


S_{max} in Ti6Al4V for different irradiation intensities



S_{min} in Al2024-T351 for different irradiation intensities

EXPERIMENTAL RESULTS



$$\frac{da}{dN} = C.K^m$$

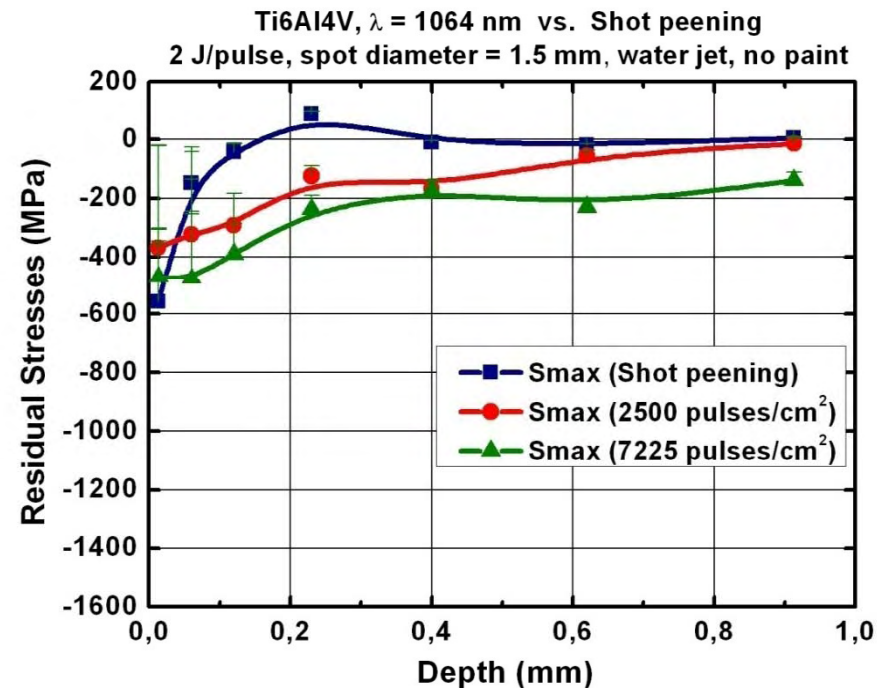
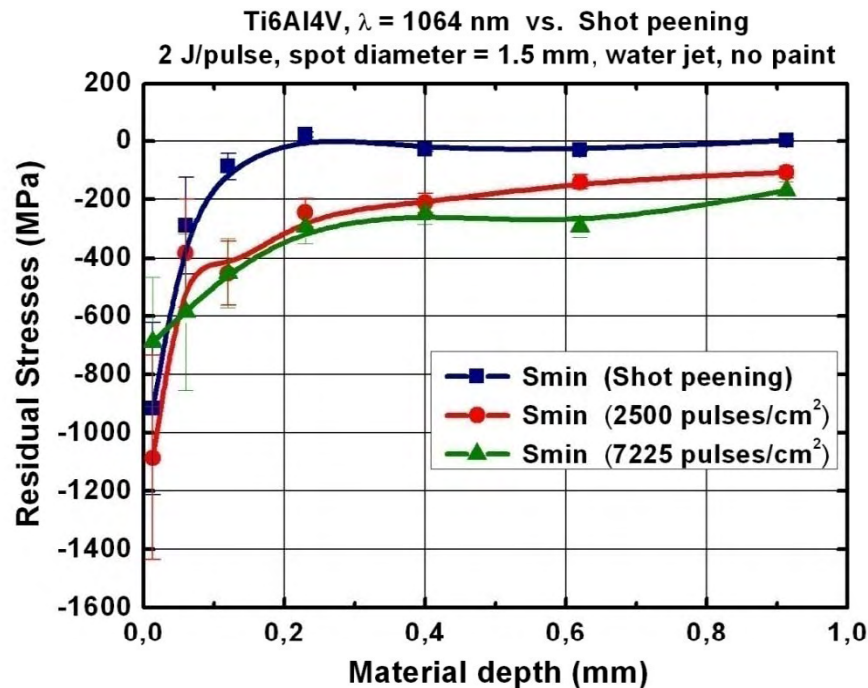
Pulse density (cm ⁻²)	C (mm/cycle)	M (dimensionless)
0 (No LSP treatment)	4x10 ⁻¹³	7.664
900	8x10 ⁻¹³	6.818
1350	2x10 ⁻¹¹	5.733
2500	3x10 ⁻¹⁰	4.723

Rubio-González, C. et al.: Mat. Sci. Eng. A., 386 (2004) 291-295

EXPERIMENTAL RESULTS

Residual Stresses (According to ASTM E837-08)

Ti6Al4V: Comparison LSP-Shot Peening



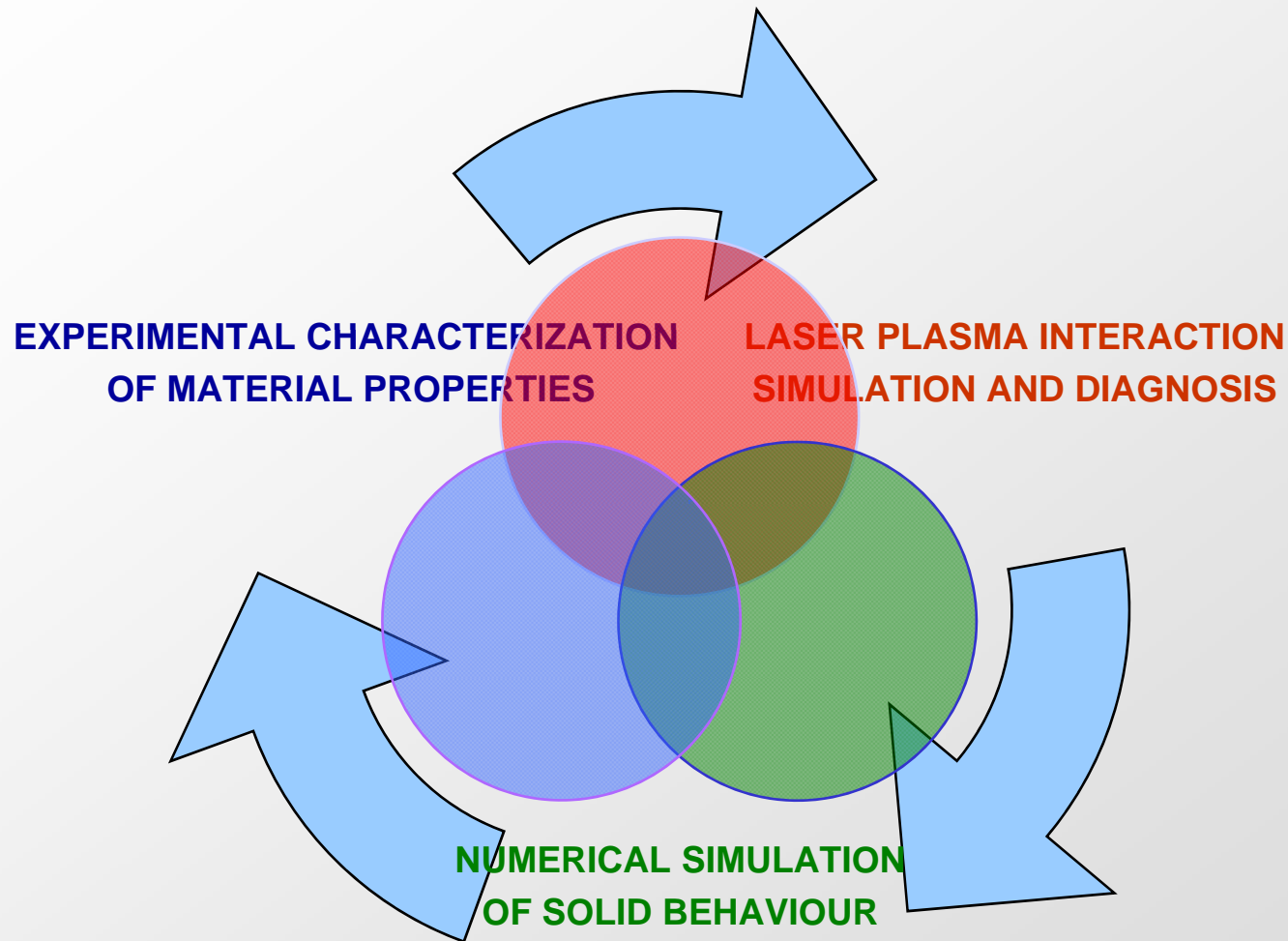
Substantial improvement in Residual Stresses
Field in Ti6Al4V vs. to Shot Peening

Decisive improvement in protected depth reached in
Ti6Al4V for different irradiation intensities

DISCUSSION AND OUTLOOK

- Important surface resistance and life cycle extension improvements in critical high reliability components by LSP have been experimentally demonstrated. The associated predictive assessment capabilities needed for adequate process design have also been developed and used for theoretical-experimental contrast.
- In view of the important improvements reached in wear behaviour, surface roughness (precursor of improved corrosion resistance) and fatigue life (all of them resulting from the deep compressive residual stresses fields introduced by the process), the LSP technique has to be recognized as a key technology for the enhancement of materials and systems durability and reliability.
- Important technological implementations of LSP in the aerospace, automotive, nuclear and biomedical sectors are under course, anticipating relevant improvements in service reliability and in material preservation and (eco-friendly) efficient use.

7. DISCUSSION AND OUTLOOK



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LSP: An Emerging Sustainability Supporting Technology

